



December 29, 2005

Mr. Robert Stone Hazardous Materials Specialist Humboldt County Health Department Division of Environmental Health 100 H Street, Suite 100 Eureka, California 95501

Re: Site Closure Evaluation

Indianola Market 7769 Myrtle Avenue Eureka, CA Project No. NC-18 LOP # 12690

Dear Mr. Stone,

This report presents a site closure evaluation for the property at 7769 Myrtle, Eureka, Humboldt County, California (site) (Figure 1), and was prepared for Mrs. Beverly Alto by Blue Rock Environmental, Inc. (Blue Rock). This report was prepared in response to the Humboldt County Division of Environmental Health (HCDEH) letter dated November 14, 2005.

## Background

Site Description

The subject site is located near the northern boundary of the City of Eureka in Humboldt County approximately 800 feet north of the intersection of Indianola Cutoff and Myrtle Avenue in a combined commercial/residential area of Eureka at approximately 25 feet above mean sea level (Figure 1). The site is located in the southern portion of a 5-acre parcel of land containing two residences, the Indianola Market, and The Alto Brothers Trucking equipment maintenance/storage yard and office.

#### Site History

The Indianola Market contained two 550-gallon capacity gasoline underground storage tanks (USTs) and one 550-gallon capacity diesel UST (Figure 2). The UST system, consisting of one 550-gallon gasoline and one 550-gallon diesel UST was constructed in 1953. At some time during the 1960s, the diesel UST was abandoned in-place and an additional 550-gallon gasoline UST was installed. The UST system was operated until September 1998, when the three USTs were closed by removal. The UST system was replaced by a single 1,000-gallon capacity aboveground gasoline storage tank, which is currently located on a concrete pad directly above the former UST excavation.

In September 1998, Christens NCI, Inc. (NCI), of Eureka, California, decommissioned and removed three USTs from the site along with associated piping, dispensers, and the dispenser island. This work was observed by the HCDEH and at the direction of the HCDEH inspector, approximately 75 cubic yards of obviously impacted soil was excavated and stockpiled at the site pending disposal. During UST removal activities, petroleum hydrocarbon stained soils were

observed and groundwater entering the excavation exhibited a sheen accompanied by hydrocarbon odors. This confirmed that an unauthorized release of petroleum had occurred. On September 29, 1998, Mr. Jerry Avila, operator of the UST system, filed an unauthorized release report at that time. After completion of UST removal and soil excavation operations, NCI personnel collected confirmation soil and groundwater samples from the excavation at locations specified by the HCDEH. Results of soil and groundwater sampling confirmed that an unauthorized release of petroleum had occurred.

Site Investigation and Corrective Action History

On October 1, 2001, Clearwater Group (Clearwater) supervised Fisch Environmental of Valley Springs, California drill five direct push borings to preliminarily investigate the onsite extent of soil and groundwater contamination resulting from the confirmed release from the former UST system. Results for this investigation and the locations of the proposed monitoring wells were presented in Clearwater's *Preliminary Subsurface Investigation Report* dated October 22, 2001. In a letter dated October 26, 2001, the HCDEH concurred with Clearwater recommendations for monitoring well locations.

On November 7, 2001, Clearwater supervised Mitchell Drilling Environmental (MDE) in installing three monitoring wells: MW-1, MW-2 and MW-3 (Figure 2). These monitoring wells were placed in locations to assess the sorbed and dissolved-phase hydrocarbon contamination associated with the UST release. Results of this investigation are presented in Clearwater's Monitoring Well Installation and Fourth Quarter 2001 Groundwater Monitoring Report dated December 13, 2001.

On October 10, 2002, Clearwater supervised MDE in drilling two monitoring wells: MW-4 and MW-5 (Figure 2). These monitoring wells were placed in locations to further assess the residual sorbed and dissolved-phase gasoline and diesel range hydrocarbon contamination associated with the UST release. Data collected during this phase of investigation are presented in Clearwater's Monitoring Well Installation and Fourth Quarter 2002 Groundwater Monitoring Report / Sensitive Receptor Survey dated November 18, 2002.

On June 10, 2003, Clearwater supervised MDE in drilling four soil borings: B-6 to B-9 (Figure 2). These borings were placed in locations to further assess the residual sorbed and dissolved-phase gasoline and diesel range hydrocarbon contamination associated with the UST release. Data collected during this phase of investigation are presented in Clearwater's *Additional Investigation Report* dated July 8, 2003.

Per HCDEH request in a letter dated July 11, 2003, Clearwater prepared and submitted a Corrective Action Plan (CAP) dated February 18, 2004. The HCDEH responded to the CAP submitted by Clearwater in a letter dated April 23, 2004 requesting corrections to the existing CAP and a response to questions contained in that letter. In May 2004, Blue Rock was retained by Mr. and Mrs. Alto to continue site work. Blue Rock subsequently submitted a brief letter report dated June 15, 2004 in response to HCDEH requests. Groundwater monitoring continued.

## Summary of Hydrogeology and Contamination

Hydrogeology

The subject site is situated on uplands above Humboldt Bay approximately 25 feet above mean sea level and is located approximately one mile east of the Pacific Ocean. Surface water drains to the east and south towards Fay Slough and Humboldt Bay. The site is underlain by Pleistocene age fluvial sediments of the Hookton Formation.

Cumulative investigation has indicated that the subsurface is composed of interbedded layers of elastic silts, sandy silts and sands (MH, ML, SW) to depths ranging from 2 to 20 feet bgs. The site is primarily underlain by sediments characterized as elastic silts (MH). The elastic silt is underlain by sandy silt (ML) and sands (SW) from about 10 to 20 feet bgs. Site cross sections are presented in Figures 2a and 2b. Boring logs are presented in Appendix A.

Groundwater is present in unconfined conditions beneath the site at depths of approximately 1.5 to 7 feet bgs with seasonal depth to water fluctuations of approximately 5.5 feet. The direction of groundwater flow historically has been calculated to be toward the southwest at gradients ranging from 0.017 ft/ft to 0.05 ft/ft.

Based on field observations and literature values, the average hydraulic conductivity of the average hydraulic conductivity of the elastic clayey silt unit (MH) is likely on the order of 10<sup>-6</sup> cm/s, the average hydraulic conductivity of the sandy silt unit (ML) is likely on the order of 10<sup>-4</sup> cm/s, and the average hydraulic conductivity of the sand unit (SW) is likely on the order of 10<sup>-2</sup> centimeters per second (cm/s) (Feeze and Cherry 1979).

### Contaminants of Concern

Historical soil and groundwater sample analytical data indicate that gasoline and diesel range hydrocarbons (TPHg, TPHd, BTEX and MTBE) are the contaminants of concern beneath the site (Tables 1, 2 & 3).

#### Potential for Contaminant Migration

Based on quarterly groundwater gradient and monitoring data collected historically, Blue Rock evaluated the extent of contamination in groundwater below the site and whether petroleum hydrocarbon are migrating or are likely to migrate.

Groundwater gradient was calculated based on static water level data collected during the last five quarterly groundwater monitoring events conducted. Groundwater flow direction has consistently been towards the southwest with gradients ranging from approximately 0.05 ft/ft to 0.017 ft/ft.

The approximate hydraulic conductivity for the elastic clayey silt unit (MH) is 0.002832 feet per day (10<sup>-6</sup> cm/s), the approximate hydraulic conductivity for the silty sand unit (SM) is 0.2835 feet per day (10<sup>-4</sup> cm/s), and the approximate hydraulic conductivity for the sand unit (SW) is 28.35 feet per day (10<sup>-2</sup> cm/s). A porosity of 35% is assumed for all soils (Freeze and Cherry, 1979).

The groundwater seepage velocity calculations for the three general material types documented at the site according to Darcy's Law follow:

## Elastic clayey silt (MH)

 $V_s = Ki/n$   $V_s = (0.002835 \text{ ft/day}) (0.05 \text{ ft/ft}) = 0.000405 \text{ ft/day}$ 0.35

Sandy silt (SM)

 $V_s = Ki/n$   $V_s = (0.2835 \text{ ft/day}) (0.05 \text{ ft/ft}) = 0.0405 \text{ ft/day}$ 0.35

Sand (SW)

 $V_s = Ki/n$   $V_s = (28.35ft/day) (0.05 ft/ft) = 4.05 ft/day$ 0.35

Where,

K (SW) = 28.35 ft/d K (MH) = 0.002835 ft/d K (SM) = 0.2835 ft/d i = 0.05 ft/ft (the max. observed at the site) n = 35%

Based on the calculations above, the maximum estimated seepage velocity for groundwater in the SW layer is 4.05 feet/day. The minimum seepage velocity within the MH strata is 0.000405 feet/day.

Despite the low solubility of hydrocarbons in water, the dominant mode of lateral contaminant migration is as a dissolved component in groundwater. The movement of groundwater is a function of naturally occurring groundwater gradient, soil permeability and anthropogenic affects of pumping and surface irrigation. Yet, the migration of dissolved-phase hydrocarbons is inhibited by natural attenuation processes of dilution, dispersion, volatilization, adsorption, and chemical and biological degradation. Based on the declining concentrations of target analytes in groundwater samples collected from MW-5 (the distal downgradient monitoring point), it is likely that a combination of these natural attenuation processes are occurring within the plume which appear to be limiting significant downgradient migration of dissolved-phase petroleum hydrocarbons in groundwater.

#### Sorbed-Phase Contamination

Historical investigation data indicate the presence of one general area of soil contamination beneath the site (Figure 4). This area appears to extend around, and beneath, the former excavation limits and former fuel dispenser at TPHg concentrations ranging to 3,600 mg/Kg and TPHd concentrations ranging to 1,200 mg/Kg with an area of approximately 780 sq. ft.

Based on cumulative soil analytical data collected to date, the estimated average residual TPHg and TPHd concentrations in soil are 723 mg/Kg and 215 mg/Kg, respectively. The resulting estimate of residual sorbed-phase TPHg and TPHd mass is approximately 563 lbs. (92.5 gal.) and 168 lbs. (27 gal), respectively.

Additionally, using the above average TPHg and TPHd residual sorbed phase concentrations as a conservative estimate for sorbed-phase hydrocarbons removed during overexcavation activities, and the size of the final excavation (approximately 75 cubic yards), Blue Rock estimates that the amount of sorbed-phase TPHg and TPHd contamination removed during the excavation activities of 1998 to be approximately 153 lbs. (25 gal.) and 45 lbs. (7 gal) respectively. Mass Calculations are presented in Appendix B

### Dissolved-Phase Contamination

Cumulative investigation indicates that the residual dissolved-phase TPHg contaminant plume is currently limited to an approximate 737 ft<sup>2</sup> area and the residual dissolved phase MTBE contaminant plume is currently limited to an approximate 7,610 ft<sup>2</sup> area. Mass calculations for dissolved phase gasoline and MTBE were calculated separately as the impacted area for each contaminant range differs. Dissolved-phase TPHg and MTBE calculations were performed using the most recent groundwater analytical results from the fourth quarter 2005. The following calculations estimate the extent of the residual mass remaining in place.

The total area for each of the two contaminants (TPHg and MTBE) was divided into separate areas as applicable according to the range of contamination present in that area. The maximum extent of the residual dissolved-phase TPHg contaminant plume in October 2005 was approximately 35 feet long (parallel to groundwater flow) and 25 feet wide (perpendicular to groundwater flow) and the maximum extent of the dissolved phase MTBE plume in October 2005 was approximately 130 feet long (parallel to groundwater flow) and 70 feet wide (perpendicular to groundwater flow).

The area containing concentrations of dissolved-phase gasoline-range contaminants (TPHg) in October 2005 was limited to a 737 ft area (zone 1). Average concentrations of dissolved-phase TPHg in this location were 330  $\mu$ g/L. The core of the plume is located near MW-2 (Figure 5a). Approximately 0.11 lb. or 0.02 of gallons of gasoline-range hydrocarbons resided in the dissolved-phase in this area (Appendix B).

The area containing concentrations of dissolved-phase MTBE contaminants in October 2005 was limited to an approximate 7,610 ft area (zones 1 through 4). Average concentrations of dissolved-phase MTBE at the plume core near MW-2 were 370  $\mu$ g/L (Figure 5b). Approximately 0.12 lbs. or 0.002 gallons of MTBE resided in the dissolved-phase in zones 1 through 4) (Appendix B).

First Order Exponential Decay Rates

Concentrations of dissolved-phase TPHg and MTBE in MW-2 have decreased consistently over the duration of the quarterly groundwater monitoring program that was initiated in November 2001. The following section discusses current first order decay rate data.

Concentrations of TPHg and MTBE for well MW-2 and MTBE for well MW-5 were plotted against time since the initial groundwater monitoring event in November 2001 (Charts 1, 2 & 3) and an exponential curve was fitted to each plot (Appendix C). The method presented by Buscheck, O'Reilly, and Nelson (1993) was used to calculate first-order decay rates by the following equation:

$$C(t) = C_0 e^{-(kt)}$$

Where,

C(t) is concentration as a function of time (t)

 $C_0$  = is concentration as t = 0

 $k = is the decay rate (t^{-1})$ 

During the most recent quarterly groundwater monitoring event, as displayed in Chart 1 and Chart 2, the TPHg first-order decay rate at MW-2 was 0.0008 day<sup>-1</sup> and first order decay rate for MTBE at MW-2 was 0.0011 day<sup>-1</sup>. Additionally, as displayed in Chart 3, the first-order decay rate at MW-5 for MTBE was 0.0016 day<sup>-1</sup>. The first-order decay rates calculated for target analytes in selected monitoring wells correlate with the lower end of published values, which typically range from 0.001 day<sup>-1</sup> to 0.01 day<sup>-1</sup> (Buscheck, O'Reilly, and Nelson 1993).

Observed Dissolved-Phase Mass Reduction

Blue Rock calculated the current dissolved-phase mass based on the groundwater analytical data obtained in the fourth quarter 2005 groundwater monitoring event. Current calculations for the dissolved-phase mass for October 2005 indicate that approximately 0.11 lbs. (0.02 gallons) of TPHg and 0.12 lbs. (0.02 gallons) of MTBE remain dissolved in groundwater beneath the site. In contrast, the dissolved-phase mass calculations for TPHg and MTBE in January 2003 were 0.4 lbs. (0.07 gallons) and 0.8 lbs. (0.14 gallons) respectively (Appendix B). Based on these calculations, the dissolved-phase mass of TPHg and MTBE has diminished since the dissolved phase plume was fully defined with the current monitoring well network. Please refer to Figures 5c and 5d for the extent of TPHg and MTBE in January 2003.

Estimate of Time to Reach Water Quality Goals

The exponential first order decay rates for TPHg and MTBE in MW-2 (Chart 1 and Chart 2) and for MTBE in MW-5 (Chart 3) were used to predict when groundwater quality goals would be reached. Using the trend line calculations as shown in Chart 1 and 2, it appears that TPHg concentrations in groundwater will reach water quality goals (i.e. TPHg <50  $\mu g/L$ ) by approximately 2013 and MTBE concentrations in groundwater will reach water quality goals (i.e. MTBE = 5  $\mu g/L$ ) by approximately 2016 based on the trendline from MW-2. Based on the trendline calculations shown in Chart 3, it appears MTBE concentrations in groundwater will reach water quality goals by approximately 2006 based on the trendline for MW-5.

Additionally, it should be noted that the residual dissolved-phase plume is stable with no significant migration. This has been evidenced by concentrations of target analytes slightly above, or below, laboratory detection limits in downgradient and cross gradient monitoring points for the duration of the quarterly groundwater monitoring program.

## Sensitive Receptor Survey Summary

In December 2002, a sensitive receptor survey was conducted by Clearwater Group and submitted with the *Monitoring Well Installation and Fourth Quarter 2002 Groundwater Monitoring Report* dated January 20, 2003. Clearwater visited the site as well as the search area to identify bodies of surface water, wetlands, and schools, to map underground utilities adjacent to the site. Clearwater searched HCDEH and DWR well records to identify well locations. Clearwater also interviewed City of Eureka Engineering and Humboldt County Public Works personnel to evaluate locations and depths of any underground utilities near the site. The following was reported by Clearwater.

The area surrounding the site is comprised of mixed residential, commercial, and rural. All homes and businesses (except Fred's Body Shop) in the search area use private wells for domestic water. The nearest downgradient domestic water well (#14 Table 4) is located at 7711 Myrtle Avenue approximately 150 feet to the west-southwest (downgradient) of monitoring well MW-5. According to the property owner the well is approximately 60 feet deep. The date of installation and the screened interval of this well are not known. Water from this well has been sampled periodically through the course of the monitoring program and has been found to be free of detectable target analytes (Table 5). Another domestic well (#15 Table 4) is present onsite and is approximately 260 feet northwest of the store. This well provides water for the Indianola Market, Alto Brothers Trucking Office, and the rental home west of the market. According to Cecil Alto, the well was installed in 1954 and is 110 feet deep. The screened interval of this well is not known. The Body Shop at the corner of Indianola Cutoff Road and Myrtle Avenue utilizes City of Eureka water. The City's water source is from a municipal well located in the Mad River.

Drainage ditches run north/south on each side of Myrtle Avenue. One drainage ditch runs along the south side of Indianola Cutoff Road. No other surface water bodies exist within the 1,000 foot search area.

The City of Eureka has a 24-inch concrete encased water main running down the center of Myrtle Avenue approximately 35 feet east of the former UST locations. The approximate depth of burial of this line is 6-8 feet bgs. PG&E gas lines enter the site on the north and south side of the market with a depth of burial not exceeding 3 feet bgs. The subject site as well as surrounding properties are served by septic systems. No other utilities are buried within the search area.

No schools or other potential sensitive receptors were identified in Clearwater's survey.

### **Summary and Conclusions**

Cumulative investigation has indicated that the subsurface is composed of interbedded layers of elastic silts, sandy silts and sands (MH, ML, SW) to depths ranging from 2 to 20 feet bgs. The site is primarily underlain by sediments characterized as elastic silts (MH). The elastic silt is underlain by sandy silt (ML) and sands (SW) from about 10 to 20 feet bgs. Site cross sections are presented in Figures 2a and 2b. Boring logs are presented in Appendix A.

Groundwater is present in unconfined conditions beneath the site at depths of approximately 1.5 to 7 feet bgs with seasonal depth to water fluctuations of approximately 5.5 feet. The direction of groundwater flow historically has been calculated to be toward the southwest at gradients ranging from 0.017 ft/ft to 0.05 ft/ft.

Historic cumulative soil and groundwater sample analytical data indicate that diesel and gasoline range hydrocarbons TPHd, TPHg, BTEX and MTBE are the contaminants of concern beneath the site (Tables 1 and 2).

It appears that site contaminants have the ability to transport through the subsurface at rates ranging from 0.000405feet/day to 4.05 feet/day using Darcy's Law. However, it appears that a combination of natural attenuation processes are occurring within the plume which is preventing significant offsite migration of petroleum hydrocarbons based on analytical results slightly above detection limits in groundwater samples collected from MW-5.

Approximately 563 lb. or 92.5 gallons of gasoline-range hydrocarbons and 168 lb. or 27 gallons of diesel range hydrocarbons remain sorbed to soil beneath the site (Appendix D) and approximately 32 gallons of sorbed-phase gasoline and diesel-range hydrocarbons were removed during overexcavation activities of 1998.

The dissolved-phase mass of gasoline range contamination was calculated at approximately 0.40 lb. or 0.07 gallons and the dissolved-phase MTBE mass was calculated at approximately 0.80 lb. or 0.14 gallons in January 2003 following the installation of MW-4 and MW-5. The most recent data indicate that the residual dissolved-phase TPHg and MTBE masses are 0.11 lb. or 0.02 gallons and 0.12 lb. or 0.02 gallons, respectively. This indicates a mass removal and/or attenuation of 0.8 gallons of dissolved-phase gasoline-range hydrocarbons since January 2003.

During the most recent quarterly groundwater monitoring event, as displayed in Chart 1 and Chart 2, the TPHg first-order decay rate at MW-2 was 0.0008 day<sup>-1</sup> and first order decay rate for MTBE at MW-2 was 0.0011 day<sup>-1</sup>. Additionally, as displayed in Chart 3, the first-order decay rate at MW-5 for MTBE was 0.0016 day<sup>-1</sup>.

The exponential first order decay rates for TPHg and MTBE in MW-2 (Chart 1 and Chart 2) and for MTBE in MW-5 (Chart 3) were used to predict when groundwater quality goals would be reached. Using the trend line calculations as shown in Chart 1 and 2, it appears that TPHg concentrations in groundwater will reach water quality goals (i.e. TPHg <50  $\mu$ g/L) by approximately 2013 and MTBE concentrations in groundwater will reach water quality goals (i.e. MTBE = 5  $\mu$ g/L) by approximately 2016 based on the trendline from MW-2. Based on the

trendline calculations shown in Chart 3, it appears MTBE concentrations in groundwater will reach water quality goals by approximately 2006 based on the trendline for MW-5.

The residual plume of dissolved-phase gasoline range hydrocarbons is stable with no significant migration. This has been evidenced by concentrations of target analytes below, or slightly above, laboratory detection limits in downgradient and cross gradient monitoring points since the dissolved-phase plume was fully defined. Although some residual sorbed-phase hydrocarbon contamination is present in the area of the former USTs, the rate of natural attenuation processes appears greater than of partitioning of sorbed-phase hydrocarbons into dissolved-phase.

Based on the sensitive receptor survey performed by Clearwater, no impact to sensitive receptors is occurring. The nearest downgradient domestic well located at 7711 Myrtle Avenue (Table 5) has remained free of detectable target analytes (Table 3). Buried utilities near the site do not appear to be acting as migratory pathways for contaminated groundwater.

#### Recommendations

- Based on the data presented in this report, Blue Rock requests that this site be evaluated for regulatory closure.
- Once concurrence with site closure is received a contingency plan for the safe handling of
  potentially impacted soil and / or groundwater that may be encountered in the event
  subsurface work occurs in the plume area.
- Following concurrence with site closure the five site monitoring wells should be destroyed.

#### References

Buscheck, T.E., O'Reilly, K.T., and Nelson, S.N. 1993. Evaluation of Intrinsic Bioremediation at Field Sites. Proceedings of the Conference of Petroleum Hydrocarbons and Organic Chemicals in Ground Water, National Groundwater Association/API, Houston, TX. November 10-12.

Freeze, R.A. and Cherry, J.A. 1979. *Groundwater*. Prentice-Hall, Inc., Englewood Cliffs, NJ, 604 p.

#### Certification

This report was prepared under the supervision of a California Professional Geologist at Blue Rock. All statements, conclusions, and recommendations are based upon published results from past consultants, field observations by Blue Rock, and analyses performed by a state-certified laboratory as they relate to the time, location, and depth of points sampled by Blue Rock. Interpretation of data, including spatial distribution and temporal trends, are based on commonly used geologic and scientific principles. It is possible that interpretations, conclusions, and recommendations presented in this report may change, as additional data become available and/or regulations change.

Information and interpretation presented herein are for the sole use of the client and regulating agency. The information and interpretation contained in this document should not be relied upon by a third party.

The service performed by Blue Rock has been conducted in a manner consistent with the level of care and skill ordinarily exercised by members of our profession currently practicing under similar conditions in the area of the site. No other warranty, expressed or implied, is made.

If you have any questions regarding this project, please contact us at (707) 441-1934.

Sincerely,

Blue Rock Environmental, Inc.

Prepared by:

Andrew LoCicero Project Scientist Reviewed by:

Brian Gwinn, PG Principal Geologist

#### Attachments

Table 1: Cumulative Soil Analytical Data
 Table 2: Grab Groundwater Analytical Data

Table 3: Groundwater Elevations and Analytical Results

Table 4: Well Construction Details

Table 5: Domestic Wells Located Within the 1,000 Foot SRS Search Area

Figure 1: Site location Map

• Figure 2: Site Plan

Figure 2a: Cross Section A-A'
 Figure 2b: Cross Section B-B'

Figure 3: Groundwater Elevations and Gradient Map – 10/11/05

Figure 4: Sorbed-Phase Hydrocarbon Distribution

Figure 5a: Dissolved-Phase TPHg Distribution – 10/11/05
 Figure 5b: Dissolved-Phase MTBE Distribution – 10/11/05
 Figure 5c: Dissolved-Phase TPHg Distribution – 1/13/03
 Figure 5d: Dissolved-Phase MTBE Distribution – 1/13/03

Appendix A: Boring Logs

Appendix B: Mass Calculations for Sorbed and Dissolved-Phase Contaminants

Appendix C: First Order Decay Rate

Cc:

Beverly Alto 7803 Myrtle Avenue Eureka, CA 95503

Jerry Avila 7769 Myrtle Avenue Eureka, CA 95503

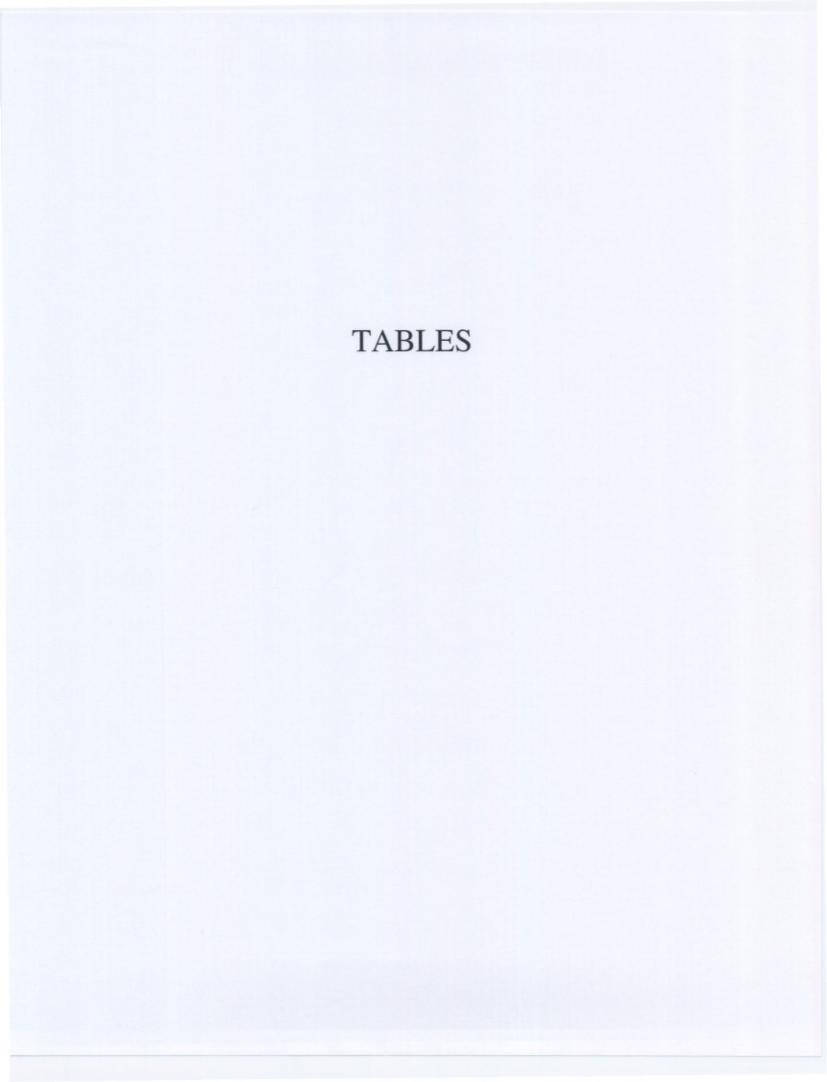


Table 1 SOIL ANALYTICAL DATA

Indianola Market 7769 Myrtle Avenue Eureka, California Project No. NC-018

	Cample							Project No. N	C-018							
Sample ID	Sample Depth (feet bgs)	Sample Date	TPHg (mg/kg)	TPHd (mg/kg)	Benzene (mg/kg)	Toluene (mg/kg)	Ethylbenzene (mg/kg)	Xylenes (mg/kg)	MTBE (mg/kg)	DIPE (mg/kg)	TAME (mg/kg)	ETBE (mg/kg)	TBA (mg/kg)	Methanol (mg/kg)	Ethanol (mg/kg)	Total Lea (μg/g)
#1		9/29/98	3,600		1.6	0.82	100	140	4.1	< 0.02	0.15	< 0.02	0.20		***	
#2	-	9/29/98	880		0.50	0.58	2.0	8.4	4.0	< 0.02	0.47	< 0.02	0.59	-	-	-
B-1	5	10/1/01	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	<0.2	< 0.01	2.9
B-1	10	10/1/01	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.2	< 0.01	4.1
B-2	4	10/1/01	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	<0.01	<0.2	< 0.02	3.4
B-2	8	10/1/01	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.01	<0.2	< 0.02	2.8
B-3	4	10/2/01	4	2.2	< 0.005	< 0.005	< 0.005	< 0.005	0.38	< 0.005	< 0.005	< 0.005	0.018	<0.2	< 0.02	6.3
B-3	7	10/2/01	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	0.25	< 0.005	< 0.005	< 0.005	0.14	<1	<0.05	5
B-4	4	10/2/01	9.4	49	< 0.005	< 0.005	< 0.005	< 0.01	0.082	< 0.005	< 0.005	< 0.005	0.043	<1	< 0.05	3.1
B-4	7	10/2/01	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	0.035	< 0.005	< 0.005	< 0.005	0.0081	<0.2	< 0.01	4.3
B-5	4	10/2/01	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	0.0074	< 0.005	< 0.005	< 0.005	< 0.005	<0.2	< 0.01	5.1
B-5	7	10/2/01	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	<0.2	< 0.01	2.7
MW-1	5	11/7/01	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	-		5.7
MW-1	10	11/7/01	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005			6.7
MW-1	15	11/7/01	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	-		5.9
MW-1	20	11/7/01	<1	<1	< 0.005	< 0.005	<0.005	<0.005	<0.005	< 0.005	< 0.005	<0.005	<0.005	-	-	5.0
MW-2	10	11/7/01	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	0.058	< 0.005	< 0.005	< 0.005	0.015	_		4.8
MW-2	15	11/7/01	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	-		6.2
MW-2	20	11/7/01	<1	<1	<0.005	<0.005	<0.005	<0.005	< 0.005	< 0.005	< 0.005	<0.005	< 0.005	-	-	4.4
MW-3	5	11/7/01	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	-		3.8
MW-3	10	11/7/01	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	-		3.6
MW-3	15	11/7/01	<1	<1	< 0.005	<0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	-		3.7
MW-4	5	10/10/02	<1	<1	< 0.005	<0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	_		-
MW-4	10	10/10/02	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005			
MW-4	15	10/10/02	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005			
MW-4	20	10/10/02	<1	<1	< 0.005	<0.005	<0.005	< 0.005	< 0.005	< 0.005	< 0.005	<0.005	< 0.005	-	-	-
MW-5	5	10/10/02	<1	<1	<0.005	<0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	_	_	-
MW-5	10	10/10/02	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005		**	**
MW-5	15	10/10/02	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005			
MW-5	20	10/10/02	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	-		

#### Table 1 SOIL ANALYTICAL DATA

Indianola Market 7769 Myrtle Avenue Eureka, California Project No. NC-018

	Sample							riojectivo. r	0.010							
Sample ID	Depth (feet bgs)	Sample Date	TPHg (mg/kg)	TPHd (mg/kg)	Benzene (mg/kg)	Toluene (mg/kg)	Ethylbenzene (mg/kg)	Xylenes (mg/kg)	MTBE (mg/kg)	DIPE (mg/kg)	TAME (mg/kg)	ETBE (mg/kg)	TBA (mg/kg)	Methanol (mg/kg)	Ethanol (mg/kg)	Total Lead (μg/g)
B-6	2	6/11/03	170	1200	0.044	<0.025	1.6	0.11	0.046	<0.025	<0.025	< 0.025	<0.25	_	_	_
B-6	4	6/11/03	100	86	0.083	< 0.025	1.3	1.1	0.79	< 0.025	< 0.025	< 0.025	<0.25	-		-
B-7	5	6/11/03	920	160	0.063	< 0.05	4.0	5.2	0.14	<0.05	< 0.05	< 0.05	<0.25	_	-	-
B-7	8	6/11/03	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	0.91	< 0.005	< 0.005	< 0.005	< 0.005	-		
B-7	10	6/11/03	100	7.1	< 0.025	< 0.025	0.25	0.42	0.29	< 0.025	< 0.025	< 0.025	< 0.25			
B-8	2	6/11/03	<1	<1	< 0.005	< 0.005	< 0.005	<0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	_		-
B-8	4	6/11/03	<1	4.2	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005			
B-8	5	6/11/03	<1	<1	< 0.005	<0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	-	-	-
B-9	10	6/11/03	<1	<1	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	< 0.005	_		

#### Notes:

mg/kg = milligrams per kilogram
TPHd: Total Petroleum Hydrocarbons as Diesel by Method 3550/8015M
TPHg: Total Petroleum Hydrocarbons as Gasoline by Method 5030/8260B
Benzene: by Method 8260B
Ethylbenzene: by Method 8260B
Xylenes: by Method 8260B
Xylenes: by Method 8260B

DIPE: Di-Isopropyl Ether by Method 8260B
TAME: Tertiary Amyl Methyl Ether by Method 8260B
ETBE: Ethyl Tertiary Butyl Ether by Method 8260B
TBA: Tertiary Butyl Alcohol by Method 8260B
Methanol: by Method 8260B
Ethanol: by Method 8260B
Total Lead: by EPA Method 6010

#### Table 2 GRAB GROUNDWATER ANALYTICAL DATA

Indianola Market 7769 Myrtle Avenue, Eureka, California Project No. NC-18

Sample ID	Sample Date	TPHd (µg/L)	TPHg (μg/L)	Benzene (µg/L)	Toluene (µg/L)	Ethylbenzene (µg/L)	Xylenes (μg/L)	MTBE (μg/L)	DIPE (µg/L)	TAME (µg/L)	ETBE (µg/L)	TBA (μg/L)	Methanol (µg/L)	Ethanol (µg/L)	Lead (µg/L)
#8	9/29/98		-	-		-	-	25,000	<50	150	64	<500	-	-	-
B-1	10/1/01	120	<50	<0.5	< 0.5	<0.5	<0.5	<0.5	<0.5	< 0.5	<0.5	<5	98	<5	<5
B-2	10/1/01	<50	<50	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<5	59	<5	<5
B-3	10/1/01	<100	<200	2.7	<2	2.3	2.2	1,900	<2	10	9.2	100	<5,600	<20	<5
B-4	10/1/01	<50	54	<0.5	<0.5	<0.5	<0.5	190	<0.5	1.7	<0.5	18	<1,100	<5	<5
B-5	10/1/01	<50	<50	<0.5	<0.5	<0.5	<0.5	41	<0.5	<0.5	<0.5	<5	<150	<5	<5
B-9	6/11/03	270	<50	<0.5	<0.5	1.7	1.7	17	< 0.5	<0.5	<0.5	<5	-	-	-

#### Notes

μg/L = micrograms per liter

"-": Not analyzed, available, or applicable

TPHd: Total Petroleum Hydrocarbons as Diesel by EPA Method 3510/8015M

TPHg: Total Petroleum Hydrocarbons as Gasoline by EPA Method 5030/8260B

Benzene by EPA Method 8260B

Toluene by EPA Method 8260B

Ethylbenzene by EPA Method 8260B

Xylenes by EPA Method 8260B

MTBE: Methyl Tertiary Butyl Ether by EPA Method 8260B

DIPE: Di-Isopropyl Ether by EPA Method 8260B

TAME: Tertiary Amyl Methyl Ether by EPA Method 8260B

TABLE : Idealy Amy seemly East by EPA Method 8260B TBA: Tertiary Buryl Ricobol by EPA Method 8260B TBA: Tertiary Buryl Alcobol by EPA Method 8260B Methanol by EPA Method 8260B Ethanol by EPA Method 8260B

Dissolved Lead by EPA Method 200.8

Table 3
GROUNDWATER ELEVATIONS AND ANALYTICAL RESULTS

Indianola Market 7769 Myrtle Avenue Eureka, California Project No. NC-18

Well No.	Sampling Date	TOC (feet)	DTW (feet)	GWE (feet)	TPHg (µg/L)	TPHd (µg/L)	Benzene (µg/L)	Toluene (μg/L)	Ethylbenzene (µg/L)	Xylenes (μg/L)	MTBE (μg/L)	DIPE (µg/L)	TAME (μg/L)	ETBE (µg/L)	TBA (μg/L)	Ethanol (μg/L)	Methanol (μg/L)
MW-1	11/20/01	99.99	5.15	94.84	<50	<50	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<5	<5	<50
	2/2/02	99.99	2.58	97.41	<50	<50	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	< 0.5	<5	<5	<50
Screen	5/2/02	99.99	2.67	97.32	<50	<50	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	< 0.5	<5	<5	<50
3'-20'	8/2/02	99.99	5.07	94.92	<50	<50	< 0.5	<0.5	<0.5	< 0.5	0.99	< 0.5	< 0.5	< 0.5	<5		_
	(10/15/02)	32.22	6.77	25.45	<50	<50	< 0.5	< 0.5	< 0.5	< 0.5	0.57	<0.5	< 0.5	< 0.5	<5		
	1/13/03	32.22	2.03	30.19	<50	<50	< 0.5	< 0.5	< 0.5	< 0.5	0.51	< 0.5	< 0.5	< 0.5	<5	**	-
	4/1/03	32.22	1.33	30.89	<50	<50	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	<0.5	< 0.5	< 0.5	<5		-
	7/10/03	32.22	4.33	27.89	<50	66	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	<5		_
	10/2/03	32.22	7.07	25.15	<50	110	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5	<0.5	< 0.5	< 0.5	<5		
	1/5/04	32.22	3.38	28.84	<50	58	< 0.5	< 0.5	< 0.5	< 0.5	2.9	<0.5	< 0.5	< 0.5	<5		
	4/6/04	32.22	2.85	29.37	<50	81	< 0.5	< 0.5	< 0.5	< 0.5	3.2	< 0.5	< 0.5	< 0.5	<5	-	-
	7/1/04	32.22	4.92	27.30	<50	<50	< 0.5	< 0.5	< 0.5	< 0.5	3.6	< 0.5	< 0.5	< 0.5	<5		
	10/1/04	32.22	7.04	25.18	<50		< 0.5	< 0.5	< 0.5	< 0.5	1.5						
	1/4/05	32.22	2.05	30.17	<50		< 0.5	< 0.5	< 0.5	< 0.5	1.6	**					
	4/18/05	32.22	2.40	29.82	<50	**	< 0.5	< 0.5	< 0.5	< 0.5	1.1						
	7/1/05	32.22	3.15	29.07	<50		< 0.5	< 0.5	< 0.5	< 0.5	0.76						
	10/11/05	32.22	5.51	26.71	<50		<0.5	<0.5	<0.5	<0.5	0.71				-	-	-
MW-2	11/20/01	99.15	4.92	94.23	300	<200	<2	<2	<2	<2	1,100	<2	5.3	4	35	<20	<200
	2/2/02	99.15	2.31	96.84	1,400	<500	<5	<5	<5	<5	1,900	<5	5.5	5.4	63	<50	<500
Screen	5/2/02	99.15	2.47	96.68	1,000	<350	3.1	<2.5	<2.5	<2.5	1,200	<2.5	5.8	5.5	33		
3'-20'	8/2/02	99.15	4.77	94.38	650	<400	<5	<5	<5	<5	2,300	<5	12	6.1	71		
	(10/15/02)	31.33	6.49	24.84	73	<100	< 0.5	< 0.5	< 0.5	< 0.5	310	< 0.5	1.9	0.84	7.7	**	
	1/13/03	31.33	1.97	29.36	1,500	<800	2.6	< 0.2	< 0.2	3.2	1,300	< 0.2	7.3	4.6	41		
	4/1/03	31.33	2.07	29.26	1,000	<1,100	<2	<2	<2	2.8	940	<2	5.4	3.4	25 1		
	7/10/03	31.33	4.09	27.24	1,100	<600	<2	<2	<2	<2	1,000	<2	5.8	4	25 1		
	10/2/03	31.33	6.80	24.53	1,000	<800	<2.5	<2.5	<2.5	<2.5	1,100	<2.5	7.7	5	32 1		
	1/5/04	31.33	2.76	28.57	1,300	<1,000	<1.5	<1.5	<1.5	<1.5	740	<1.5	<1.5	4	22		
	4/6/04	31.33	2.58	28.75	280	120	< 0.5	< 0.5	< 0.5	< 0.5	120	< 0.5	0.72	0.82	<5		
	7/1/04	31.33	4.56	26.77	510	690	<1.5	<1.5	<1.5	<1.5	800	<1.5	7.10	2.4	27		
	10/1/04	31.33	6.71	24.62	<50	<50 <sup>2</sup>	< 0.5	< 0.5	< 0.5	< 0.5	130				**		-
	1/4/05	31.33	1.85	29.48	580	<80 <sup>2</sup>	<1.5	<1.5	<1.5	<1.5	580						
	4/18/05	31.33	2.08	29.25	620	<500 <sup>2</sup>	<1.0	<1.0	<1.0	<1.0	510	**					-
	7/1/05	31.33	2.57	28.76	420	<400 <sup>2</sup>	< 0.5	< 0.5	< 0.5	< 0.5	260			**			-
	10/11/05	31.33	5.21	26.12	370	<80 <sup>2</sup>	< 0.5	<0.5	<0.5	<0.5	370	-	-	-	-	-	-
MW-3	11/20/01	99.30	3.36	95.94	<50	<50	<0.5	<0.5	<0.5	<0.5	100	<0.5	0.85	<0.5	8.1	<5	<50
	2/2/02	99.30	1.56	97.74	<50	<50	< 0.5	< 0.5	< 0.5	< 0.5	2.4	< 0.5	< 0.5	< 0.5	<5	<5	<50
Screen	5/2/02	99.30	1.67	97.63	<50	<50	< 0.5	< 0.5	< 0.5	<0.5	6	< 0.5	< 0.5	< 0.5	<5		
3'-20'	8/2/02	99.30	3.37	95.93	<50	<50	< 0.5	< 0.5	< 0.5	< 0.5	89	<0.5	0.65	< 0.5	5.3		-
	(10/15/02)	31.47	5.06	26.41	<50	<50	< 0.5	<0.5	< 0.5	< 0.5	94	<0.5	0.79	< 0.5	<5		-
	1/13/03	31.47	1.44	30.03	<50	56	< 0.5	< 0.5	Page 15 of 3	< 0.5	340	< 0.5	2.1	< 0.5	27		-

# Table 3 GROUNDWATER ELEVATIONS AND ANALYTICAL RESULTS

Indianola Market 7769 Myrtle Avenue Eureka, California Project No. NC-18

Well	Sampling	TOC	DTW	GWE	TPHg	TPHd	Benzene	Toluene	Ethylbenzene	Xvlenes	MTBE	DIPE	TAME	ETBE	TBA	Ethanol	Methanol
No.	Date	(feet)	(feet)	(feet)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)	(µg/L)
MW-3	4/1/03	31.47	1.37	30.10	51	<50	<0.5	<0.5	<0.5	<0.5	280	<0.5	2	<0.5	18		
IVI W -J	7/10/03	31.47	2.80	28.67	<50	89	<0.5	<0.5	<0.5	<0.5	89	<0.5	0.84	<0.5	6.4		-
Screen	10/2/03	31.47	5.41	26.06	<50	150	<0.5	<0.5	<0.5	<0.5	110	<0.5	0.71	<0.5	<5	_	_
3'-20'	1/5/04	31.47	2.46	29.01	<50	<50	<0.5	<0.5	<0.5	<0.5	11	<0.5	<0.5	<0.5	<5		
3-20	4/6/04	31.47	1.71	29.76	<50	<50	< 0.5	<0.5	<0.5	<0.5	0.73	<0.5	<0.5	< 0.5	<5		
	7/1/04	31.47	3.16	28.31	<50	<50	<0.5	<0.5	<0.5	<0.5	80	<0.5	<0.5	<0.5	<5		
	10/1/04	31.47	5.26	26.21	<50		< 0.5	<0.5	<0.5	<0.5	61	**			-		
	1/4/05	31.47	1.43	30.04	<50	_	<0.5	<0.5	<0.5	<0.5	9						
	4/18/05	31.47	1.48	29.99	<50	_	<0.5	<0.5	<0.5	<0.5	2.2				_		
	7/1/05	31.47	1.01	30.46	<50		<0.5	<0.5	<0.5	<0.5	1.4						
	10/11/05	31.47	3.88	27.59	<50		<0.5	<0.5	<0.5	<0.5	18	_	-				-
MW-4	10/15/02	32.74	4.99	27.75	<50	<50	<0.5	<0.5	<0.5	<0.5	4.1	<0.5	<0.5	<0.5	<5		
IVI W -4					1 (5)							<0.5		<0.5	<5		-
C	1/13/03	32.74 32.74	1.41	31.33	<50	<50	<0.5	<0.5	<0.5	<0.5	0.92	<0.5	<0.5 <0.5	<0.5	<5		-
Screen	4/1/03		1.45	31.29	<50	<50	<0.5	<0.5	<0.5	< 0.5	0.70						
3'-20'	7/10/03	32.74	2.82	29.92	<50	<50	<0.5	<0.5	<0.5	<0.5	7.9	<0.5	<0.5	<0.5	<5	-	-
	10/2/03	32.74	5.32	27.42	<50	99	<0.5	<0.5	<0.5	< 0.5	6.9	<0.5	<0.5	<0.5	<5	-	-
	1/5/04	32.74	2.60	30.14	<50	<50	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<5	-	-
	4/6/04	32.74	1.88	30.86	<50	<50	< 0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<5		44
	7/1/04	32.74	3.19	29.55	<50	<50	<0.5	<0.5	<0.5	<0.5	17	<0.5	<0.5	<0.5	<5	-	-
	10/1/04	32.74	5.16	27.58	<50	-	<0.5	<0.5	<0.5	<0.5	6.3		-			-	-
	1/4/05	32.74	1.52	31.22	<50		<0.5	<0.5	<0.5	<0.5	0.68		-		-		
	4/18/05	32.74	1.66	31.08	<50		< 0.5	<0.5	<0.5	<0.5	<0.5		**		-	**	
	7/1/05	32.74	1.98	30.76	<50	**	< 0.5	<0.5	<0.5	<0.5	< 0.5	**					
	10/11/05	32.74	3.69	29.05	<50	-	<0.5	<0.5	<0.5	<0.5	3.4	-	-		-	-	-
MW-5	10/15/02	29.71	7.11	22.60	<50	<50	< 0.5	< 0.5	<0.5	< 0.5	32	< 0.5	<0.5	<0.5	<5		-
	1/13/03	29.71	0.66	29.05	<50	<50	< 0.5	< 0.5	< 0.5	< 0.5	31	< 0.5	< 0.5	< 0.5	<5		
Screen	4/1/03	29.71	1.75	27.96	<50	<50	< 0.5	< 0.5	< 0.5	< 0.5	35	< 0.5	< 0.5	< 0.5	<5		**
5'-20'	7/10/03	29.71	4.60	25.11	<50	<50	< 0.5	< 0.5	< 0.5	< 0.5	20	< 0.5	< 0.5	<0.5	<5		-
	10/2/03	29.71	7.45	22.26	<50	<50	< 0.5	< 0.5	< 0.5	< 0.5	9	< 0.5	< 0.5	< 0.5	<5		-
	1/5/04	29.71	2.31	27.40	<50	85	< 0.5	< 0.5	< 0.5	< 0.5	29	< 0.5	< 0.5	< 0.5	<5		-
	4/6/04	29.71	2.53	27.18	<50	68	< 0.5	< 0.5	< 0.5	< 0.5	38	< 0.5	< 0.5	< 0.5	<5		-
	7/1/04	29.71	4.95	24.76	86	86	< 0.5	< 0.5	<0.5	< 0.5	170	< 0.5	1.4	0.97	17		
	10/1/04	29.71	7.26	22.45	<50	<50 <sup>2</sup>	< 0.5	< 0.5	< 0.5	< 0.5	2	**					-
	1/4/05	29.71	0.78	28.93	<50	<50 <sup>2</sup>	< 0.5	< 0.5	< 0.5	< 0.5	5.3						-
	4/18/05	29.71	2.02	27.69	<50	<50 <sup>2</sup>	< 0.5	< 0.5	< 0.5	< 0.5	8.2						
	7/1/05	29.71	3.27	26.44	<50	<50 <sup>2</sup>	< 0.5	< 0.5	<0.5	< 0.5	92					**	
	10/11/05	29.71	5.72	23.99	<50	<50 <sup>2</sup>	< 0.5	< 0.5	< 0.5	< 0.5	5.6					**	-

## Table 3 GROUNDWATER ELEVATIONS AND ANALYTICAL RESULTS

Indianola Market 7769 Myrtle Avenue Eureka, California Project No. NC-18

Well No.	Sampling Date	TOC (feet)	DTW (feet)	GWE (feet)	TPHg (μg/L)	TPHd (μg/L)	Benzene (μg/L)	Toluene (µg/L)	Ethylbenzene (µg/L)	Xylenes (μg/L)	MTBE (µg/L)	DIPE (µg/L)	TAME (µg/L)	ETBE (µg/L)	TBA (µg/L)	Ethanol (µg/L)	Methanol (μg/L)
Dom - 1	4/1/03	(Domestic we	ell located at 77	11 Myrtle Ave.)	<50	<50	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<0.5	<5	_	_
	1/4/05				<50	<50	< 0.5	< 0.5	< 0.5	< 0.5	< 0.5			**			
	10/11/05				<50	<50	< 0.5	<0.5	< 0.5	< 0.5	<0.5	-			-		-
				MCL		_	1	150	300	1,750	5						
			Taste & oc	dor threshold	5	100		42	29	17	5						
		NO	CRWQCB o	leanup goals	<50	100	0.50	42	29	17	5						

Notes

TOC: Top of casing referenced to mean sea level (4.33 NAVD 88 (NGS LV 0638) SS rod E1401 1988

Sample date in parentheses indates new wellhead survey per Geotracker

DTW: Depth to water as referenced to benchmark.

GWE: Ground water elevation as referenced to benchmark

μg/L=micrograms per liter

"--": Not analyzed, available, or applicable

MCL: Maximum contaminant level, an enforceable drinking water standard

Taste & odor threshold: A drinking water standard

1. Tert Butanol results may be biased high (see case narative in laboratory report)

2. TPHd analysis performed using silica gel eleanup

TPHg: Total Petroleum Hydrocarbons as Gasoline by Method 5030/8260B TPHd: Total Petroleum Hydrocarbons as Diesel by Method 3510/8015M

MTBE: Methyl Tertiary Butyl Ether by Method 8260B

DIPE: Di-Isopropyl Ether by Method 8260B

TAME: Tertiary Amyl Methyl Ether by method 8260B ETBE: Ethyl Tertiary Butyl Ether by Method 8260B TBA: Tertiary Butyl Alcohol by Method 8260B

NCWQCB: North Coast Water Quality Control Board

Table 4
Well Construction Details
Indianola Market

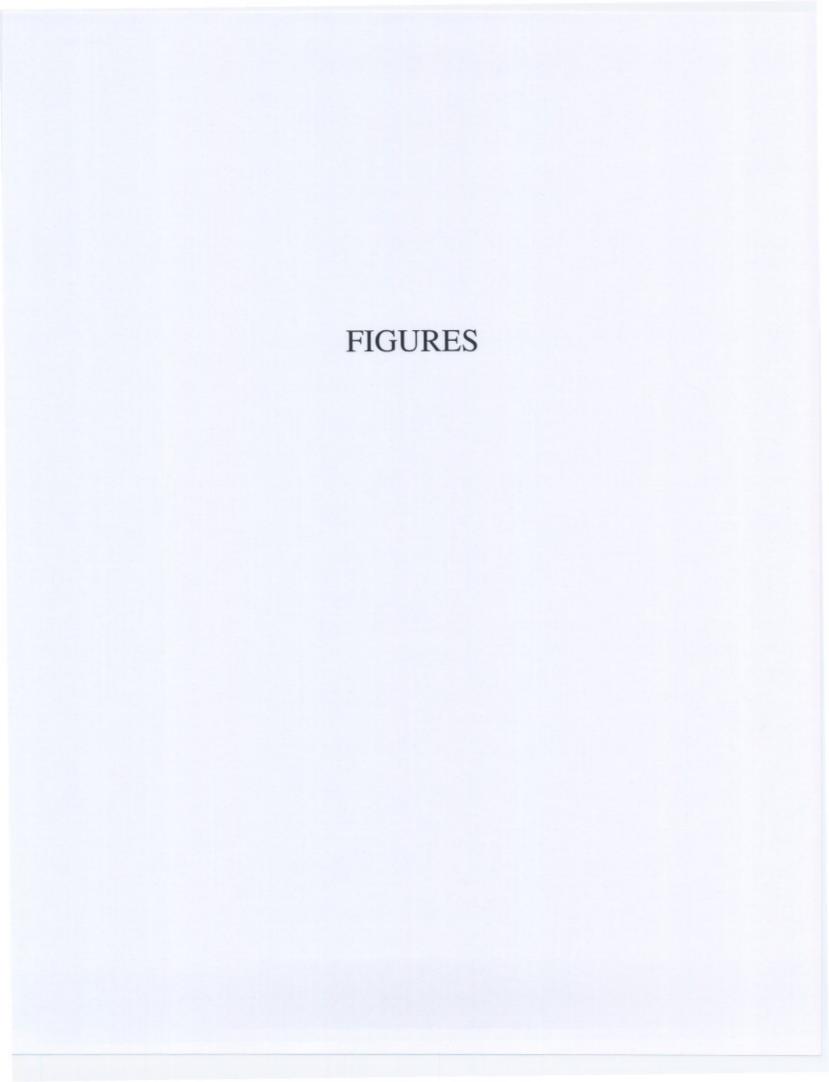
Indianola Market 7769 Myrtle Avenue Eureka, CA Project # NC-18

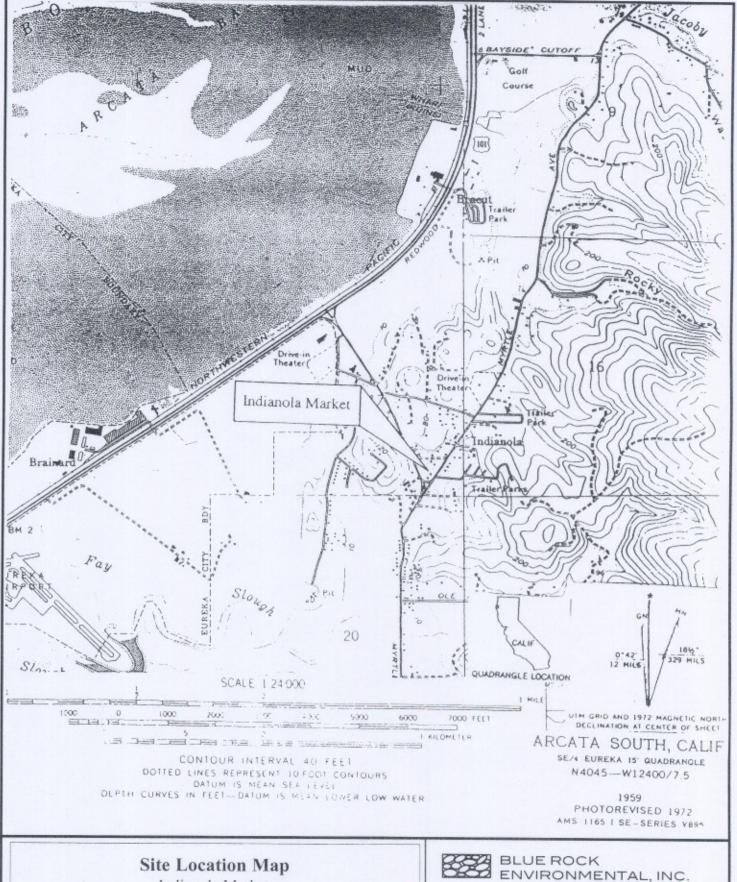
Well Identification	Date Intstalled	Intstalled by	Casing Diameter (inches)	Total Depth (feet)	Blank Interval (feet)	Screened Interval (feet)	Slot Size (inches)	Filter Pack (feet)	Bentonite Seal (feet)	Cement (feet)
MW-1	10/10/01	Clearwater	2	20	0-3	3-20	0.02	2-20	1-2	0-1
MW-2	10/10/01	Clearwater	2	20	0-3	3-20	0.02	2-20	1-2	0-1
MW-3	10/10/01	Clearwater	2	20	0-3	3-20	0.02	2-20	1-2	0-1
MW-4	10/7/02	Clearwater	2	20	0-3	3-20	0.02	2-20	1-2	0-1
MW-5	10/7/02	Clearwater	2	20	0-3	5-20	0.02	2-20	1-2	0-1

# Table 5 Domestic Wells Located Within the 1,000 Foot SRS Search Area

Indianola Market 7769 Myrtle Avenue Eureka, CA 95503 Project # NC-18

Well ID	Well Adress	Well Use	Year Installed	Depth of Well (feet)	Screened Interval-Slot Size
1	531 Indianola Road	Domestic	1988	153 feet	150-153 feet (3/16")
2	Rt. 1 Box 275 Old Arcata Road	Domestic	1966	120 feet	None
3	Rt. 1 Box 430 Old Arcata Road	Domestic/Irrigation	1973	155 feet	136-148 feet (0.018")
4	Old Arcata Road corner of Indianola	Domestic/Irrigation	1970	90 feet	74-80 feet (0.018")
5	7728 Indianola Road	Domestic	1991	191 feet	180-191 feet (4" & 3/4")
6	Indianola Road	Domestic	1962	82 feet	12 perf per row, 4 rows per foot
7	Old Arcata Road	Domestic/Irrigation	1971	80 feet	60-80 feet (3/16")
8	3855 Newell Road	Domestic	1985	220 feet	200-220 feet (5/32")
9	Rt. 1 Box 424 Bayside	Domestic	1975	115 feet	105-110 feet (3/16")
10	Indianola Cutoff Road	Domestic/Irrigation	1971	106 feet	100-106 feet (Gator 6 foot screen)
11	Old Arcata Road	Domestic	1970	169 feet	162.5-170.5 feet (#5 chisel)
12	Box 410 Bayside	Domestic/Irrigation	1968	100 feet	80-86 feet (1,000-18,000 slots)
13	Rt. 1 Box 265 Old Arcata Road	Domestic	1979	85 feet	(0.0018 sand screens)
14	7711 Myrtle Ave	Domestic	before 1950	60 feet	unknown
15	7769 Myrtle Ave	Domestic	1954	110 feet	unknown





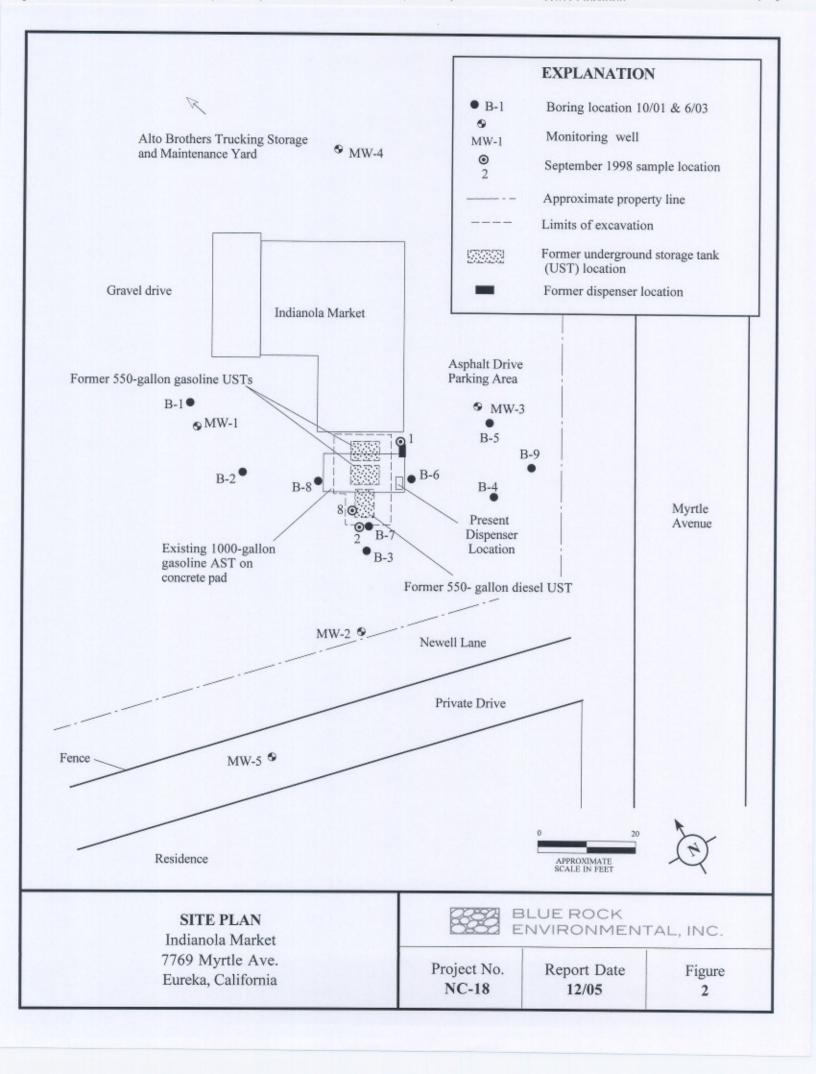
Indianola Market 7769 Myrtle Avenue Eureka, California

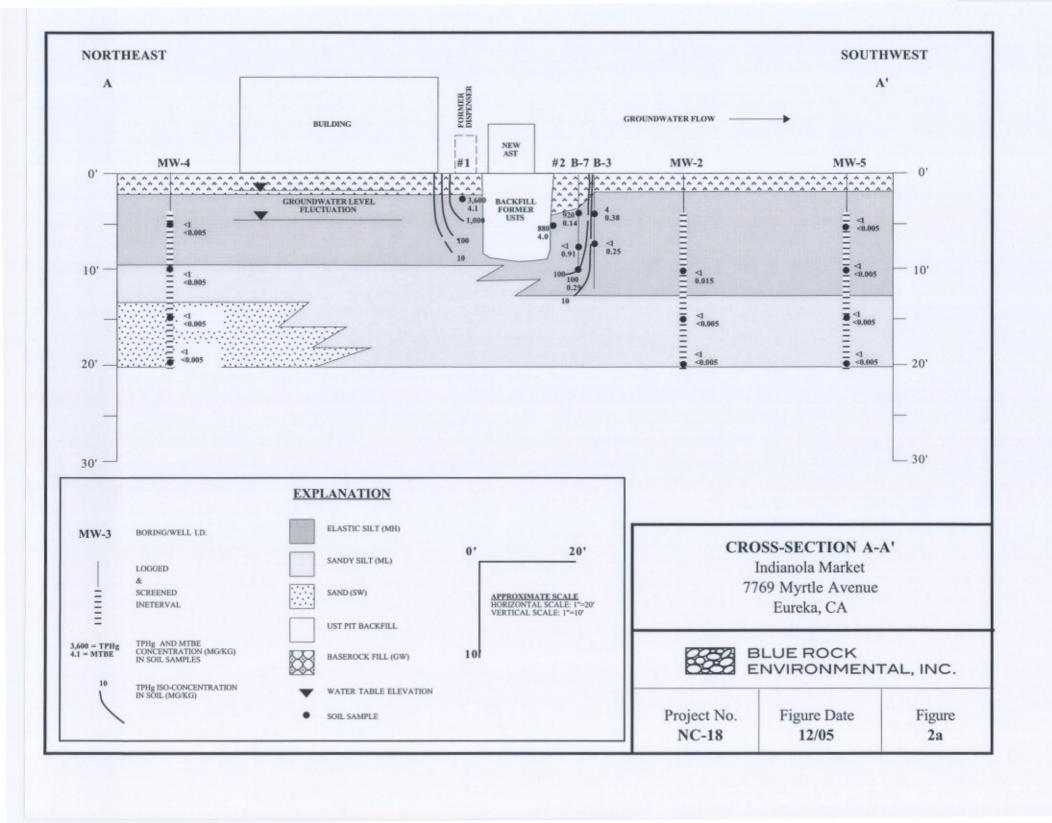


Project No. NC-18

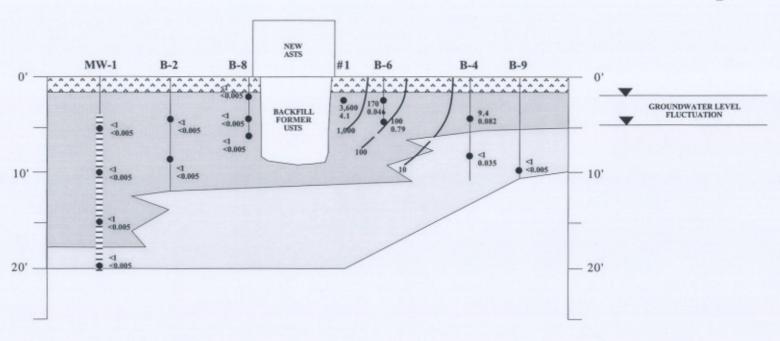
Date 12/05

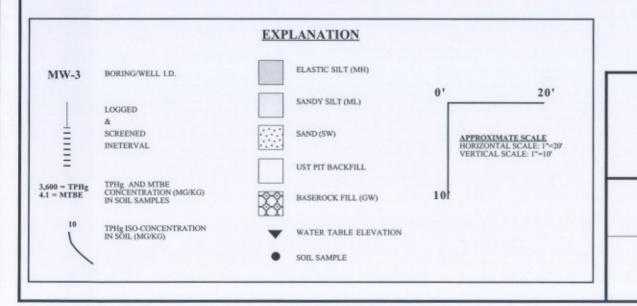
Figure 1





B'





## CROSS-SECTION B-B'

Indianola Market 7769 Myrtle Avenue Eureka, CA

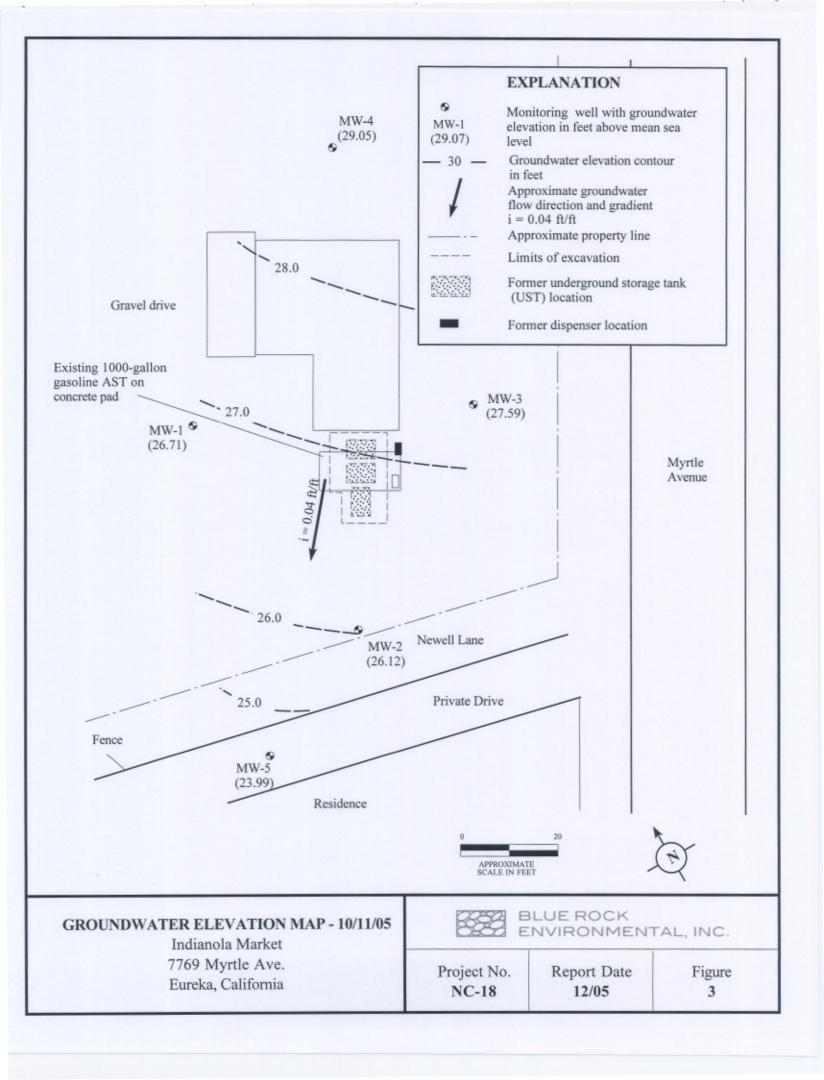


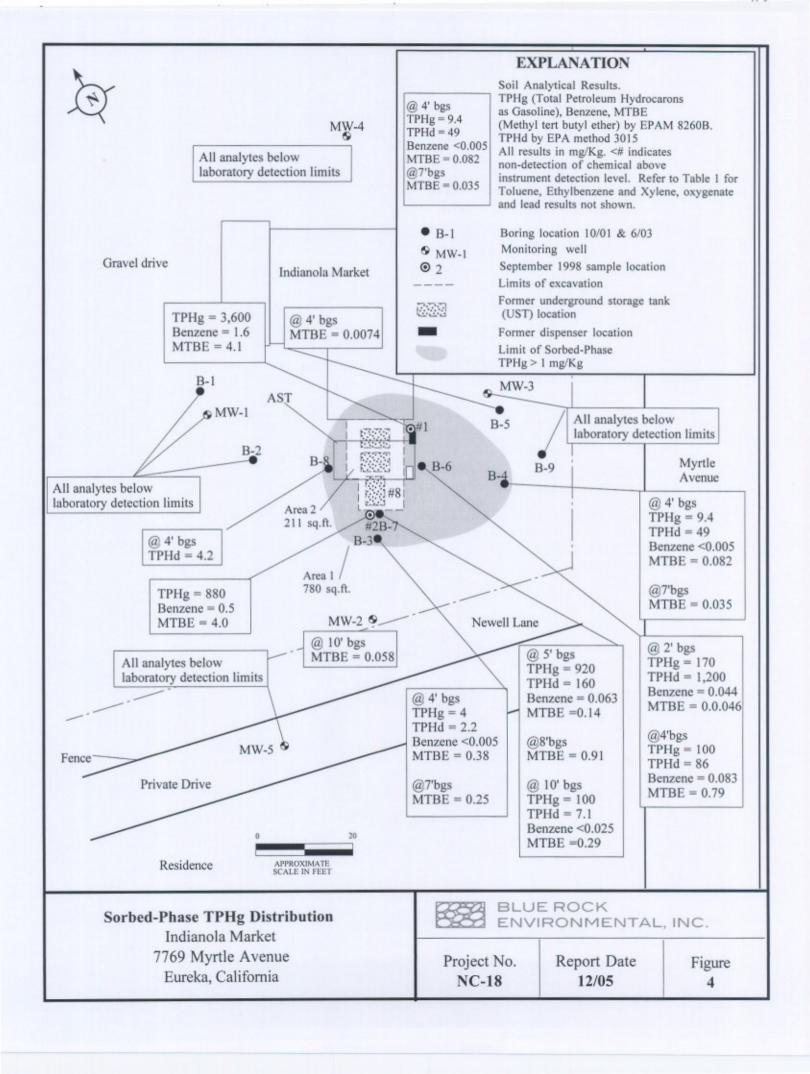
BLUE ROCK ENVIRONMENTAL, INC.

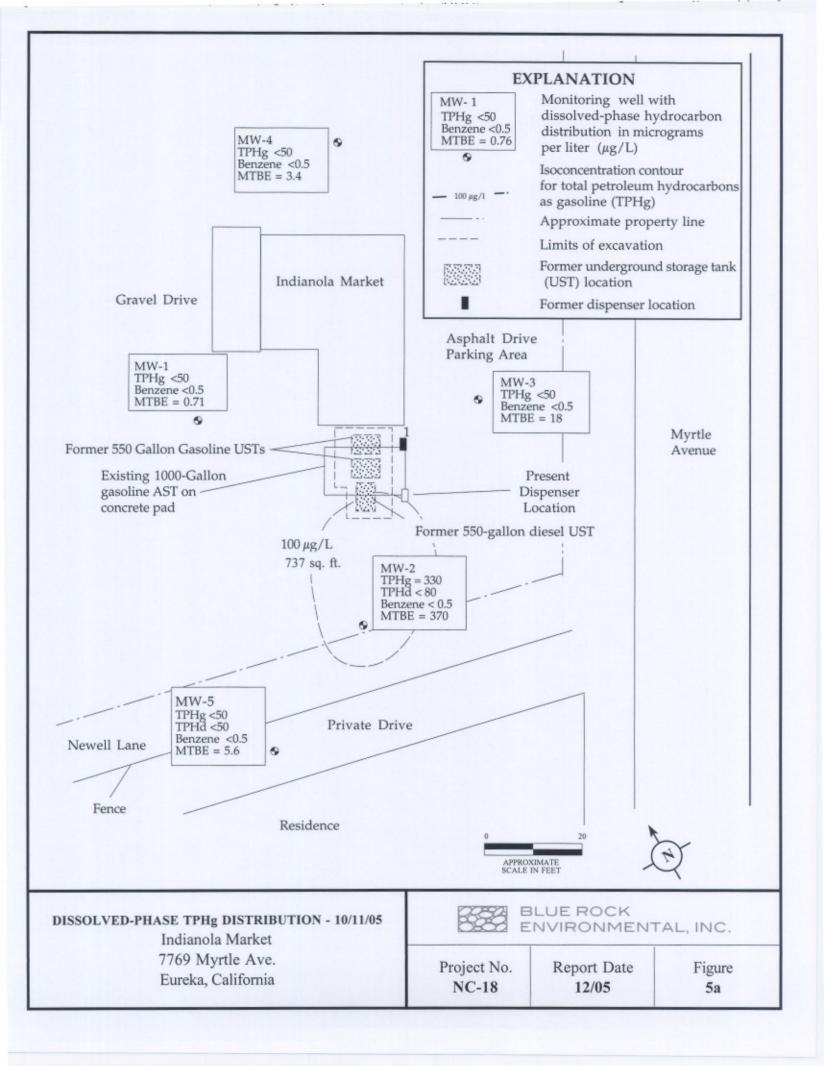
Project No. NC-18

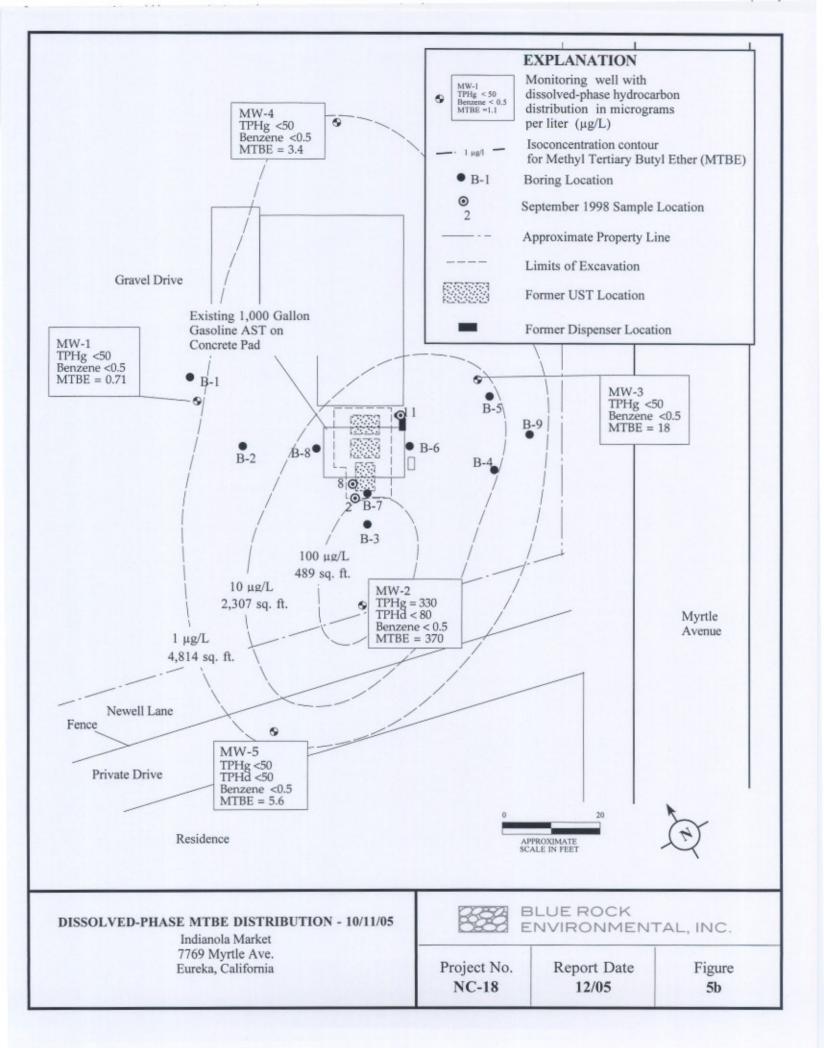
Figure Date 12/04

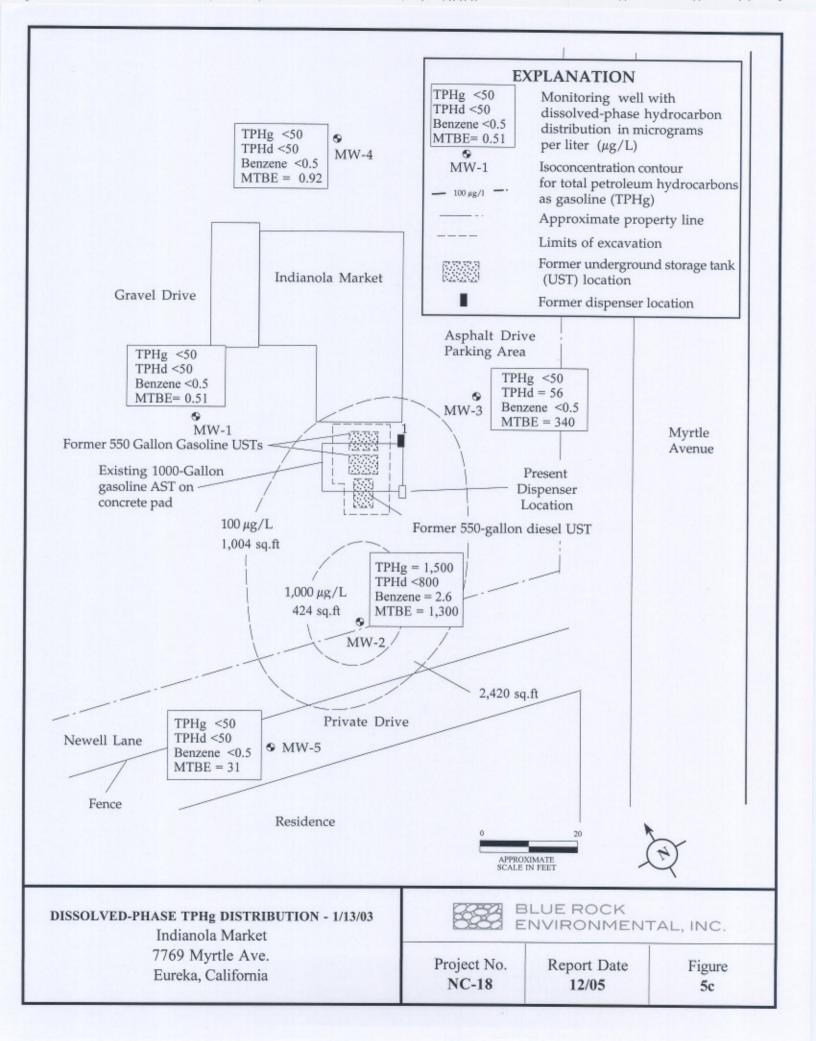
Figure 2b

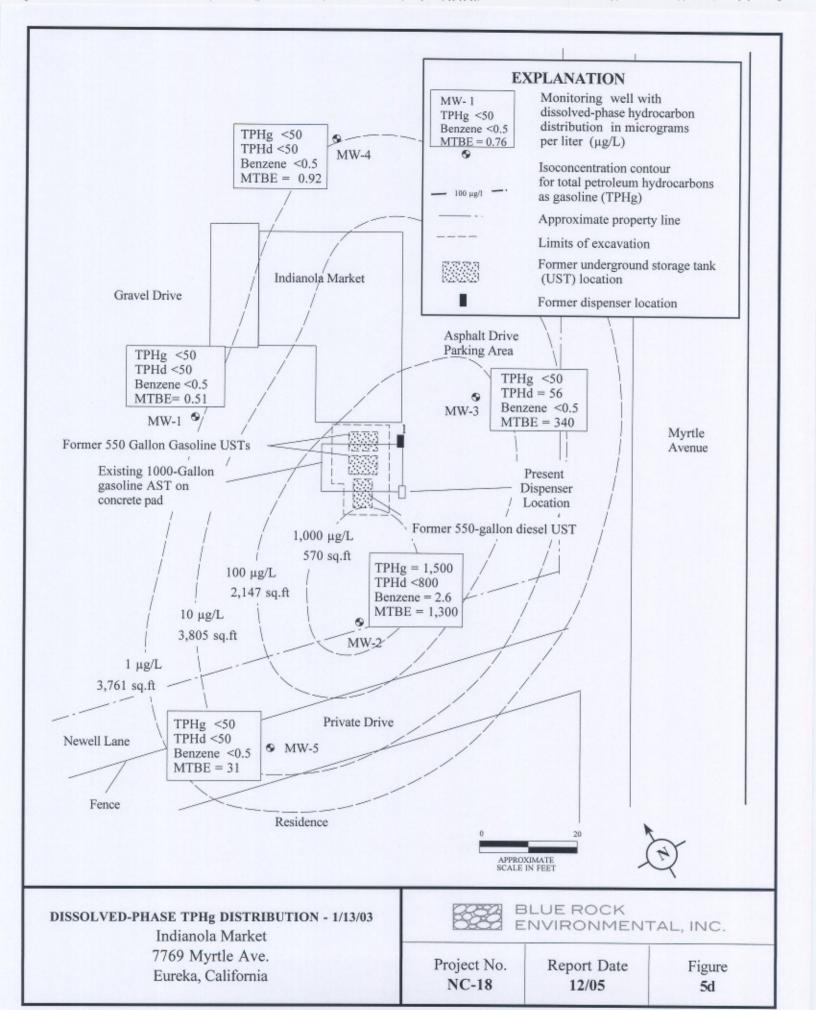














Sheet \_1\_ of \_5\_

FIELD LOCAT	TON O	F BO	RIN	NG:			CLIENT				1	PLANNED USE: Soil / GW Samp	BORING DEPTH: 12'	B-1
● B-1					1		Fisch				ental	Geoprobe	WELL DEPTH: N/A	BORING DIAMETER:
	4	1	_		N		Ric Ric		PERAT	OR:		WELL MATERIAL: N/A	FILTER PACK: N/A	SCREEN SLOT SIZE: N/A
	Fort	ner	U	ST	Locati	on	WELL S	EAL	Во	orin	g backfi	lled w/ hydrated be	entonite	
NO	SAN	(PLI					U		TIMAT				Direct Push	
Ē	5 7		25	CAL			NDIN				07	MONITORING INSTRUMEN	VT: PID	
WELL CONSTRUCTION DETAIL	BLOWS/6" INTERVAL	DRIVE	RECOVERY	ANALYTICAL	WATER	DEPTH (FEET)	OVM READING (PPM)	GRAVEL	9	FINES	GRAPHIC LOG	FIRST ENCOUNTERED WA		1'
¥88	37	DR	RB	2	E K	DE CE	96	8	SAND	E	6 0.0.0.0.0	STATIC WATER DEPTH - I	DATE: 7.07' 1	.0/02/01
						1					00000	Gravel / Sul	ograde Fill (C	GW)
						-								
		H		$\vdash$		-	-							
		П				3 —								
						4 -						Danua Class	TATA	Madamata Diagticitus
		H	-	X		5 —	0.1					Moist, No C	ey Siit (Miri),	Moderate Plasticity
						6 —					********	Wioist, No C	doi	
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				$\Box$		, -								
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				Х		10 —	0.5							
		H		H	¥			-	-	-				
					=	11 —					1////	Sandy Clay	(SC), Modera	ate Plasticity
						12 —					A::N::N::N::	Wet, No O	dor	
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		П				14 —								
		Н		Н		15 —								
						16 —								
	-	H	_	Н		17 —	-	-	-	-	-			
						18 —								
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						20 —							,	
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						23 —				-				
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						27 —								
		-	-	H		28 —		-	-	-	-			
						29 —								

Sheet \_\_2\_\_ of \_\_5\_

	FIELD LOCA	TION O	F B	ORI	NG:			CLIENT					PLANNED USE:	BORING DEPTH:	BORING/WELL NO.:
			_	_	_			-	o/I	_	-		Soil / GW Samp	12'	B-2
		1				N		Fisch				ental	Geoprobe	WELL DEPTH: N/A	BORING DIAMETER:
4:00	•B-2	1	1	_		14		DRILL I		PERAT	ror:		WELL MATERIAL:	FILTER PACK:	SCREEN SLOT SIZE:
4	B-2	For		- 11	cr	Locat		Ric	-				N/A	N/A	N/A
		ron	ilici		31	Locat	ion	WELL S	EAL:	В	orin	g backfi	lled w/ hydrated b	entonite	
FINISH	NO	SAN	MPL.	INC				U		TIMAT		1		Direct Push	
	E	.s.		RY	CAL			NDIN				N N	MONITORING INSTRUMEN	NT: PID	
0	WELL CONSTRUCTION DETAIL	BLOWS/6" INTERVAL	SIVE	RECOVERY	ANALYTICAL	WATER	DEPTH (FEET)	OVM READING (PPM)	GRAVEL	SAND	FINES	GRAPHIC LOG	FIRST ENCOUNTERED WA	0,	Manual Control of the
3:00	308	EZ	D	28	2	EX	E.	96	5	- S	E		STATIC WATER DEPTH - I	7.01' 10	0/02/01
					H		1 -					0000	Gravel / St	abgrade Fill (C	GW)
TX.	1				H		2 -								
STA	1						3 —								
DRILLING/WELL CONSTRUCTION: START					X		4 -	3.0			-				
CC							5 —	2.0					Brown Clay	ey Silt (MH),	Moderate Plasticity
STR												errererer errerer	Moist, No (	Jdor	
8					Н		6					*******			
VELL							7 —	~~				ellellelle			
VG/		-	H		X	_	8 —	0.7		-					
TEL						¥	9 —					en e			
DR		¥													
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A. Locicero 10/2/01							11 —					7777	6 1 6	(00) 16 1	. DI
0			H		Н		12					77777	Sandy Clay	y (SC), Moder	ate Plasticity
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cer					H						-	-			
OCI							14 -								
니							15 —					-			
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Sheet \_3\_ of \_5\_

,[	FIELD LOCAT	non o	F B	ORI	NG:			CLIENT					PLANNED USE: Soil / GW Samp	BORING DEPTH:	BORING/WELL NO.:
			-	_				DRILLIN		_			DRILL RIG TYPE:	WELL DEPTH:	BORING DIAMETER:
						1		Fisch					Geoprobe	N/A	3'
11:00		N	7			N		DRILL R	ug of	ERAT	OR:		WELL MATERIAL:	FILTER PACK:	SCREEN SLOT SIZE:
7	/			В	-3			Ric	k				N/A	N/A	·N/A
	Former U	ST Lo	cat					WELL S	EAL:	Во	oring	g backfi	lled w/ hydrated be	entonite	
FINISH	Z	SAN	MPL	INC	3					TMAT			SAMPLING METHOD:	Direct Push	
1	OE .			>	3			DING				200	MONITORING INSTRUMEN	NT: PID	
	WELL CONSTRUCTION DETAIL	BLOWS/6	/E	RECOVERY	ANALYTICAL	EER	EF	OVM READING (PPM)	GRAVEL	9	83	GRAPHIC LOG	FIRST ENCOUNTERED WA	TER DEPTH: 6'	
10:00	DET	35	DRI	REC	Š	WATER	DEPTH (FEET)	NA NA	SE	SAND	FINES		STATIC WATER DEPTH - I	DATE: 5.94' 1	0/02/01
7					Н							0000	Gravel / Sub	grade Fill (G	W)
		7			Н		. —								
t	1			F	H		2 —								
STA							3 —	0.5							
DRILLING/WELL CONSTRUCTION: START					X		4 -	2.7					Grove Classes	Cile OATD	Andarota Plantinita
RUC			-	-	H		5 —						Moist HC C	Odor, stained	Moderate Plasticity
ESV							6 —						Moisi, me	odoi, builliod i	аррошинос
TTO							7 —	0.8							
/WE		X							-						
IING			-		H		8								
DRIL			F		H		9 —								
=							10 —								
72/			-		H		11 —						Drown Clay	vov. Cile (MIII)	Wat No Odor
10							12 —					Hillin.	Biowii Cia	yey Siit (Miri)	, Wet, No Odor
Locicero 10/2/01							13 —								
Cic							14 —								
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Sheet \_4\_ of \_5\_

.	FIELD LOCAT	пом о	F B	ORING	:		CLIENT					PLANNED USE:	BORING DEPTH:	BORING/WELL NO.:
			_		1		-	-	ndia	-		Soil / GW Samp	12'	B-4
	N						Fisch				ental	Geoprobe	WELL DEPTH: N/A	BORING DIAMETER:
12:00		4	4		1	3-4	DRILL F		PERAT	OR:		WELL MATERIAL:	FILTER PACK:	SCREEN SLOT SIZE:
7		For	me	TOIL	Locat	ion	Ric					N/A	N/A	N/A
		Poli	inci	031	Local	ion	WELL S	EAL:	Во	orin	g backfi	lled w/ hydrated be	entonite	
FINISH	z	SAN	(PL	ING					TIMAT			SAMPLING METHOD:	Direct Push	
Ī	OILO			CAL			DING				907	MONITORING INSTRUMEN	vr: PID	
	WELL CONSTRUCTION DETAIL	BLOWS/6" INTERVAL	VE	RECOVERY	E. E.	£E.	OVM READING (PPM)	GRAVEL	9	BS	GRAPHIC LOG	FIRST ENCOUNTERED WA	TER DEPTH: 1	<u>'</u>
11:00	E S ME	32	DRIVE	AN.	WATER	(FEET)	89	8	SAND	FINES	8	STATIC WATER DEPTH - I	DATE: 5.04' 10	0/02/01
7						1 —					00000	Gravel / Subg	grade Fill (GW	V)
	1											Dark Brown	Clayey Silt Cl	lay (MH),
TH.				-		2 —						Moderate Pla	sticity, Moist,	, HC Odor
DRILLING/WELL CONSTRUCTION: START				X		3 —	0.9							
NOL						4 -	0.9					Moist, Slight	Silt(MH), Mo	derate Plasticity
RUC						5 —					7////	Worst, Stight	HC Odoi	
SNO						6 —								
ELL				x		7 —	2.7				1////			
G/W						8 —						Silty sand (M	(I) moist mo	derate plasticity,
ILEN						9 —						No Odor	iii), moist, mo	derate plasticity,
DR						10 —								
10					Ţ									
272					-	11					1////			
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A. Locicero 10/2/01						14								
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## CGI - FIELD EXPLORATORY SOIL BORING LOG

Sheet \_5\_ of \_\_5\_

,[	FIELD LOCAT	TON O	F BC	ORII	NG:		_	CLIENT					PLANNED USE:	BORING DEPTH:	BORING/WELL NO.:
							B-5	DRILLIN	iG CO		CTOR		Soil / GW Samp	12' WELL DEPTH:	BORING DIAMETER:
								Fisch				ental	Geoprobe		3'
1:00	N	4	1					Ric Ric		ERAT	OR:		WELL MATERIAL: N/A	FILTER PACK: N/A	SCREEN SLOT SIZE: N/A
		For	mer	U	ST	Locat	ion	WELL S	EAL:	Во	orin	g backfi	lled w/ hydrated b	entonite	
FINISH	z	SAM	ФLI	INC					EST	TIMAT	ED		SAMPLING METHOD:	Direct Push	
1	e e				Y.			DING				907	MONITORING INSTRUME	NT: PID	
	JI.	VS/6 RVAL	В	WER	Ĕ	E .7	н.	REAL	TEL	0	50	HIC	FIRST ENCOUNTERED WA	TER DEPTH: 7.	5'
12:00	WELL CONSTRUCTION DETAIL	BLOWS/6" INTERVAL	DRIVE	RECOVERY	ANALYTICAL	WATER	DEPTH (FEET)	OVM READING (PPM)	GRAVEL	SAND	FINES	GRAPHIC LOG	STATIC WATER DEPTH -		
			H		H							00000	Gravel / Subg	rade Fill (GW	7)
					H		1 —								
							2 —					111111111	Brown Claye	y Silt (MH), N	Moderate Plasticity
TART			H		H		3 —						Moist, No Oc	lor	
DRILLING/WELL CONSTRUCTION: START					x		4 -	0.6				********			
OFF			H		H							111111111			
THUS.					口		5 —								
SNO					H		6 —					*******			
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FIELD LOCA	TION OF B	ORING	2:		CLIENT	o/I			a	PLANNED USE: monitoring	BORING DEPTH: 20'	BORING/WELL NO.: MW-1
•			1		DRILLI	NG CC	NTR/	СТО	t:	DRILL RIG TYPE:	WELL DEPTH:	BORING DIAMETER:
MW-	A		N		Mito				g	hollow stem	20'	8" SCREEN SLOT SIZE:
	Former	r UST	Locat	ion		Mit				pvc	2/12	0.20
					WELL	ent:	ce	mei	nt / bent	onite		
NO	SAMPL				Q		TIMA'		0		split spoon	
RUCT	1/6" /AL	ERY			SADIN	,			070	MONITORING INSTRUME	110	
WELL CONSTRUCTION DETAIL	BLOWS/6" INTERVAL DRIVE	RECOVERY	WATER	DEPTH (FEET)	OVM READING (PPM)	GRAVEL	SAND	FINES	GRAPHIC LOG	STATIC WATER DEPTH - 1		2.5'
700	m & D	2 4	27	DE	06	Ü	S	E				
1 2986				1 —					00000	Gravel / Sul	ograde Fill (G	W)
2,000				2 —								
				3 —								
	16	6		4 -	0.15							
	4 6 4 6 5 6	6 x		5 —	247							
	5 6	6		6 —						Brown Clay	ev Silt (MH)	Moderate Plasticit
				7 —			-			Moist, No o	dor	Wioderate Flasticit
				s —								
				9 —					*******			
	6 6	6 6 x 6		10 —	165				*******			
	66	6		11 -								
			_	12 —								
			÷	13 —								
	13 6	6		14 —								
	16 6	6 x		15 -	162							
	200			16 —								
				17 —								
				18 —								
	15 66	5		19						Sandy Clay (	C) Madamat	Diostinita
	15 6 c 50/56 c	6 X		20	103	-			2////	Sandy Clay (S Wet, No Odo	r	Plasticity
				21 —						, , , , , ,		
				22 —								
				23 —								
				24 —								
				25								
				26								
				27								
				28 -								
		+		29								
				30								

Sheet \_2\_ of \_3\_

FIELD LOCA	non of	BORI	NG:			Alto					monitoring	BORING DEPTH:	MW-2
		Δ		A N		Mitc					hollow stem	WELL DEPTH: 20'	BORING DIAMETER:
	Fe			ST Lo	cation	Ed I	Mito	hell			PVC PVC	FILTER PACK: 2/12	SCREEN SLOT SIZE: 0.20
	•		W-2	!						t / bento			
NOL	SAMI	PLING				9		TIMAT		8	SAMPLING METHOD: MONITORING INSTRUM	split spoon  NT: PID	
TRUCT	S/6	VERY	ANALYTICAL	ps .	-	EADD	EL			GRAPHIC LOG	FIRST ENCOUNTERED W	1110	2'
WELL CONSTRUCTION DETAIL	BLOWS/6" INTERVAL	DRIVE	ANAL	WATER	DEPTH (FEET)	OVM READING (PPM)	GRAVEL	SAND	FINES		STATIC WATER DEPTH -		
25.53		66666666			1 — 2 — 3 — 4 — 5 — 6 — 7 — 7	105				0 0 0 0	Gray -Gree	bgrade Fill (G n Clayey Silt ( lasticity, Mois prox. 1/2"	(MH),
	7 12 10	666666666666	x	<b>Y</b> .	8 — 9 — 10 — 11 — 12 — 13 — 14 — 15 — 16 — 17 — 18 — 19 — 19	9.8					Moderate P Cobbles <1	/2" ty Sand (ML),	st, Slight HC Odor  Low Plasticity
	50/5	66	X		20 — 21 — 22 — 23 — 24 — 25 — 26 — 27 — 28 —	67							

## CGI - FIELD EXPLORATORY SOIL BORING LOG

Sheet 3 of 3

FIELD LO	CATION	OF	BOR	UNG:	1		-	o/Ir	ndia	nola		PLANNED USE: monitoring	BORING DEPTH: 20'	BORING/WELL NO.: MW-3
					N	MW-3	Mitc					hollow stem	WELL DEPTH: 20'	BORING DIAMETER:
		7	_				Ed l	Mitc				WELL MATERIAL:  pvc	FILTER PACK: 2/12	SCREEN SLOT SIZE: 0.20
Form	er US	T L	oca	tion			WELL S	EAL:	ce	mei	nt / bent	onite		
-	SA	AMP	LIN	G				EST	TIMAT	TED		SAMPLING METHOD:	split spoon	
WELL CONSTRUCTION DETAIL			1	.VI			OVM READING (PPM)	Pi	ERCEN	VT.	8	MONITORING INSTRUME		
L STRU	9/SMOTE	NA PE	RECOVERY	ANALYTICA	ER ER	EF	(REAL	VEL	0	S	GRAPHIC LOG	FIRST ENCOUNTERED WA	ATER DEPTH: 10	0.0'
NON	35	DRIVE	REO	AN	WATER	DEPTH (FEET)	AND APPA	GRAVEL	SAND	FINES		STATIC WATER DEPTH -	DATE:	
	5		5 6	X		1 — 2 — 3 — 4 — 5 —	45				0000	Gray -Greei	bgrade Fill (G	MH),
	5			X	<b>T</b>	6 — 7 — 8 — 9 —	63.					Moderate P	ey Silt w/ San	t, HC Odor
		6		X		11 — 12 — 13 — 14 —						Moderate Pl	asticity, Moist	t, Slight HC Odor
		6 6 6 8 6 8 6	16	X		15 — 16 — 17 — 18 —	128					Grav Siltv	Sand (ML), L	ow Plasticity
	7 50/	56	6	X		20 — 21 — 22 — 23 —	90					Wet, No C	Odor	
						24 — 25 — 26 — 27 — 28 — 29 — 29 — 29 — 29 — 29 — 29 — 29								

#### CGI - FIELD EXPLORATORY SOIL BORING LOG

N

FIELD LOCATION OF BORING:

12:30

HSINE

11:00

LOCGED BY: M. Richard 10/10/02 DRILLING/WELL CONSTRUCTION: START

APPROVED BY:

WELL CONSTRUCTION DETAIL

MW-4

Market

R

SAMPLING

2 6 6

34 6 6

1466 2666

66 X

BLOWS/6" INTERVAL

Former UST Location

ANALYTICA

WATER

11

15

17 18

21 22 23

26 27 .

28

30

RECOVERY

Project No. BE001C 3 of 3 Sheet CLIENT/LOCATION: PLANNED USE: BORING/WELL NO .: BORING DEPTH: MW-4 Alto / Indianola monitoring 20' DRILLING CONTRACTOR: DRILL RIG TYPE: WELL DEPTH: BORING DIAMETER: Mitchell Drilling hollow stem 20' 8" DRILL RIG OPERATOR: WELL MATERIAL: FILTER PACK: SCREEN SLOT SIZE: 2/12 0.20pvc Ed Mitchell WELL SEAL: cement / bentonite SAMPLING METHOD: ESTIMATED CA mod. split spoon PERCENT OVM READING (PPM) GRAPHIC LOG MONITORING INSTRUMENT: PID FIRST ENCOUNTERED WATER DEPTH: 10.0 (FEET) SAND STATIC WATER DEPTH - DATE: 4.99' 10/15/02 Gravel / Subgrade Fill (GW) Clayey Silt (MH), dark brown <5% sand moderate to high plasticity, moist, no odor, hard 95 Clayey Silt w/ fine grain sand (MH), Rust brown moderate to high plasticity, moist, no odor, hard 70 30 Silty sand (ML), Rust brown moderate to low plasticity, moist, no odor, very dense 12 . 03 90 Sand (SW), Gray little or no fines, low plasticity, wet, no odor, very dense 24 .

Sheet \_\_3\_\_ of \_3\_

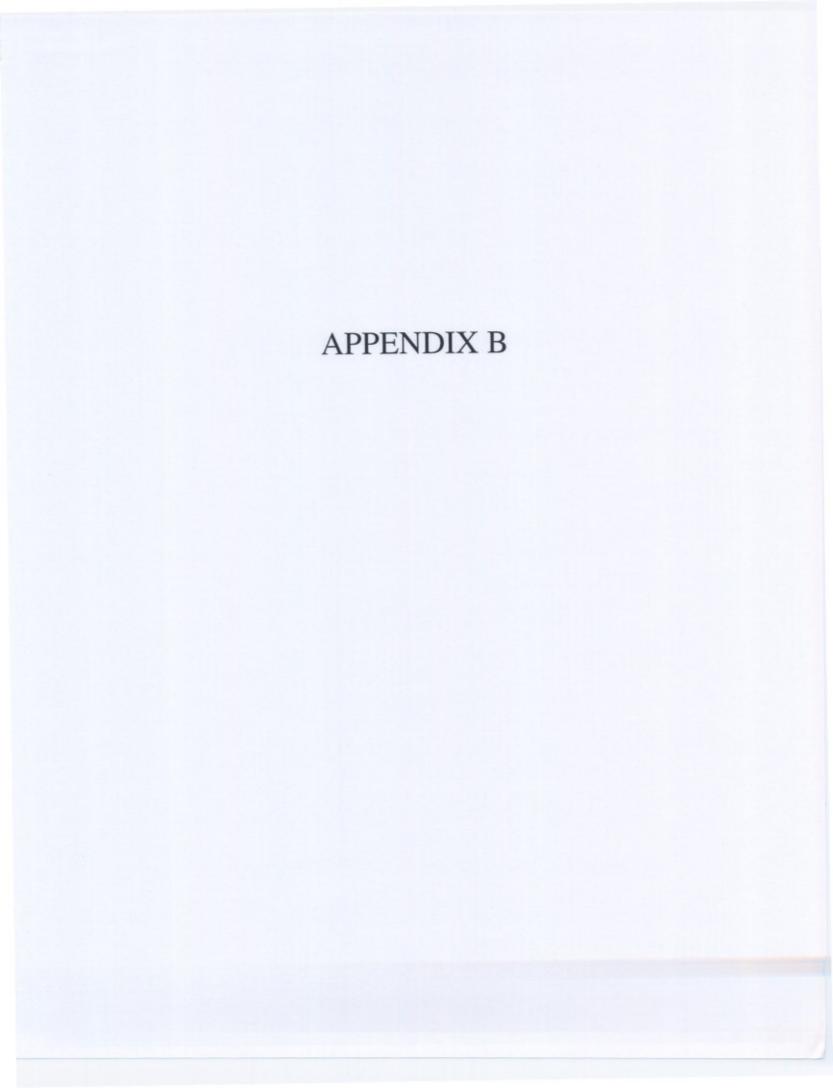
												Sh	neet3 of _3_
1	FIELD LOCAT	ION OF BO	ORING:	<b>A</b>		CLIENT	/LOCA				PLANNED USE: monitoring	BORING DEPTH:	BORING/WELL NO.: MW-5
9:30		Mark	et	N		Mitc					DRILL RIG TYPE: hollow stem	WELL DEPTH: 20'	BORING DIAMETER:
6		N				DRILL B	-	AND DESCRIPTION OF	_		WELL MATERIAL:	FILTER PACK:	SCREEN SLOT SIZE:
	Former UST Lo		•			Ed :	Mitc	hell			pvc	2/12	0.20
	MW		MW-2			WELL S	EAL:	cei	men	t / bento	onite		
FINISH		SAMPLI	ING					TMAT			SAMPLING METHOD:	CA mod. spli	t spoon
E	WELL CONSTRUCTION DETAIL		1			OVM READING (PPM)	PE	RCEN	П	8	MONITORING INSTRUME		
8:00	RUC	JVAL VAL	E G	~	_	EAD	12			IIC I	FIRST ENCOUNTERED WA		0.0'
00	FELL	BLOWS/6* INTERVAL DRIVE	RECOVERY	WATER	(FEET)	VM PM)	GRAVEL	SAND	FINES	GRAPHIC LOG	STATIC WATER DEPTH -		1' 10/15/02
	300	商会 口	2 4	33	DE.	0.5	6	OS					
					1 —						Gravel / Sul	ograde Fill (G	W)
	7084				2 —						clavey cilt	(MH) met be	own, <5% sand
F											moderate to	high plasticity	y, Moist, no odor,
DRILLING/WELL CONSTRUCTION: START					3 —						very stiff		, ,
NO					4 -								
B		5 6 6 6 30 6	6 x		5 —	0.0	-		95				
STR		30 6	6 ^										
8			H	_									
WELL				¥	7 —								
NG/					8 —						alayay silt	(MIL) must be	50/ cond
מורדש					9 —						moderate nl	asticity, moist	own, <5% sand
		9 6	6	Ā	10 —	0.0			95		very stiff	asucity, moist	, no odor,
/02		9 6 14 6 20 6	6 X	=	10	,					very suit		
10/10/02		2010	0		11								
10/					12 -								
P					13 —						0.14	M ) !	Io Diosticita
Richard											Wet, no odd	ML), gray bro	wn, low Plasticity
Ric		106	6		14 —	-					Wel, no out	or, delise	
M.		21 6	6 x		15	20		60	40				
		26 6	0		16 —								
60					17 —								
LOCGED BY:													
2		20 6	6		18								
		15 6	6		19								
- 1	LEI	16 6	6 X		20 —	0.6							
					21 —								
					22 —					-			
					23 —								
					24 —		-		-	-			
					25 —								
								-	-				
					26 —				_				
87.					27 —								
APPROVED BY:					28 —	-	-			-			
PRO					29 —								
AP			-					-	-	-			
					30 —					1			

1	FIELD LOCAT	TON O	F BORIN	G:	A N	CLIENT		ndia		ı	PLANNED USE: soil investigation	BORING DEPTH:	BORING/WELL NO.: B-6
				•	14	Mito					DRILL RIG TYPE: hollow stem	WELL DEPTH: N/A	BORING DIAMETER:
10:15			7	B-6		Ed!		chell			WELL MATERIAL: N/A	FILTER PACK: N/A	SCREEN SLOT SIZE: N/A
		For	mer US	T Locat	ion	WELL S	EAL:	ce	men	nt / bento	onite		
FINISH	NO	SAN	APLING			ų,	EST P	TIMAT ERCEN	TED	()	SAMPLING METHOD: MONITORING INSTRUMEN	split spoon	
	WELL CONSTRUCTION DETAIL	Ve.	74	ANALYTICAL WATER LEVEL		OVM READING (PPM)				GRAPHIC LOG	FIRST ENCOUNTERED WA	1110	untan ann ann atan d
	TAIL TAIL	BLOWS/6" INTERVAL	DRIVE	WATER LEVEL	DEPTH (FEET)	M RE	GRAVEL	9	ES	APH	FIRST ENCOUNTERED WA	TER DEPTH: INO W	vater encountered
3:6	M 8 M	22	RE D	2 39	图图	NA PA	ğ	SAND	FINES	5	STATIC WATER DEPTH - I	DATE:	
7					1 —					00000	Gravel / Sul	ograde Fill (C	W)
		P	66 66		2 —	165							
LART		P	66		3 —								
6/11/03 DRILLING/WELL CONSTRUCTION: START	-	P	66	_	4-	247					Gray clayey	silt (MH), M	oderate Plasticity
OFF		P	66 66	X	5 —						Moist, HC C	odor	
STRL			H	-	, -								
8					6 -								
MELL					7 -								
NG			H	-	8 —					-			
RILLI				7	9 —					1			
0					10 —								
0					11 -								
E				-		-			-				
1				7	12 —								
610					13								
Locicero				7	14 -								
			H	-	15 —		-			-			
K					16 —								
LOCCED BY:					17 —								
XXCE									-	1			
3				7	18 —			-		-			
					19 —								
1			H		20								
				7	21 —	-	-	-	-	-			
				7	22 —								
1					23 —								
				-			-	-	-	-			
				7	24 —				-				
					25 —								
					26 —						-		
3		-		-	27 —		-	-	-	-			
/EDB					28 —								
APPROVED BY:									-				
AP		-		-	29 —	-	-	-	-	-			
					30								

							1							Sheet 2 of 4
1	FIELD LOCAT	TON O	F BC	ORING:		N	Alto			nola		PLANNED USE: soil investigation	BORING DEPTH:	B-7
						14	Mitc					DRILL RIG TYPE: hollow stem	WELL DEPTH: N/A	BORING DIAMETER:
1:30		4	1				DRILL F	ug of	ERAT	OR:		WELL MATERIAL: N/A	FILTER PACK:	SCREEN SLOT SIZE:
7		East	•	B-	7 Locat		Ed		hell			IVA	N/A	N/A
		POF	mer	051	Locat	ion	WELL S	EAL:	ce	men	it / bento	onite		*
HINISH	Z	SAN	MPLI	ING					TIMAT ERCEN			SAMPLING METHOD:	split spoon	
1	WELL CONSTRUCTION DETAIL			CAL			OVM READING (PPM)				GRAPHIC LOG	MONITORING INSTRUMEN	u: PID	
	L ISTRI	BLOWS/6" INTERVAL	DRIVE	RECOVERY	E E	Ĕ.E	( REA	WEL	е	83	PHIC	FIRST ENCOUNTERED WAT	TER DEPTH: approx	c. 9.5' bgs
70.07	NE CONTRACTOR	38	DRI	NEC AN	WATER	DEPTH (FEET)	844	GRAVEL	SAND	FINES	25	STATIC WATER DEPTH - I	DATE:	
		/				1 — 2 — 3 —						Gravel / Sub	ograde Fill (C	GW)
ULLIVO DRILLING/WELL CONSTRUCTION: START		P P	6	6 X 6		5 —						Moist, old ga	asoline odor	oderate Plasticity
/WELL		P	6	6 6 x 6		7 —						Gray silty sa Moist, old g	and (ML), Mo asoline odor	oderate Plasticity
LING		P	6	6		8								Moderate Plasticity
O DRIE		P P	6	6 6 x	¥	9 —						Moist, sligh	t odor	
111						11 -								
5						12 —								
2						13 —								
						14 —								
3														
1						15 —					-			
						16 —								
LOCGED BY:						17 —								
ğ						18 —								
						19 —			-					
1						20 —			-	-				
	-					21 —			-					
						22 —								
					1	23 —								
		-	-		-			-	-	-	-			
					-	24 -					-			
						25 —				-				
						26 -								
ik.		-	+		-	27 —		-	-	-	-			
/FD B			-			28 -								
APPROVED BY:						29 -								
AF			+						-		-			
						30 -				1				

												The state of the s		Sheet 3 of 4
1	FIELD LOCA	non c	OF BC	RING	1	N		o/I	ndia	nola		PLANNED USE: soil investigation	BORING DEPTH:	B-8
13:00			٨				Mito	chell	Dri	llin	g	DRILL RIG TYPE: hollow stem	WELL DEPTH: N/A	BORING DIAMETER:
1	B-8		7				Ed	Mita				WELL MATERIAL: N/A	FILTER PACK: N/A	SCREEN SLOT SIZE:
		For	mer	UST	Locati	ion	WELL S	EAL:	ce	mer	nt / bento	onite		-
FINISH	WELL CONSTRUCTION DETAIL	SAI	MPLI	T.			U	EST P	TIMAT	TED VT		CONTRACTOR STATE OF THE STATE O	split spoon	
	DO .	507		Z Z			N N				9	MONITORING INSTRUMEN	A AL.	
12:00	NSTR TAIL	BLOWS/6" INTERVAL	12	RECOVERY	WATER	E.E.	4 RE	GRAVEL	9	19	GRAPHIC LOG	FIRST ENCOUNTERED WA	TER DEPTH: NO W	ater encountered
12	E 0 M	NE	DRIVE	A REC	WA LEV	DEPTH (FEET)	OVM READING (PPM)	GRA	SAND	SINE	\$	STATIC WATER DEPTH - D	DATE:	
APPROVED BY: A. LOGICETO 6/11/03 DRILLING/WELL CONSTRUCTION; START		P P P P P P P P P P P P P P P P P P P	66666	6 5 6 X		1 — 2 — 3 — 4 — 5 — 6 — 7 — 8 — 9 — 10 — 11 — 12 — 13 — 14 — 15 — 16 — 17 — 18 — 20 — 21 — 22 — 23 — 24 — 25 — 26 — 27 — 28 — 28 — 29 — 30 — 30 — 30 — 30 — 30 — 30 — 30 — 3							grade Fill (G	w) oderate Plasticity

								351-32601					-336.5		Sheet 4 of 4
1	FIELD LOCAT	ION O	F BK	ORII	NG:		1	CLIENT	/LOC/				PLANNED USE: soil investigation	BORING DEPTH: 10'	B-9
							N	Mito					DRILL RIG TYPE: hollow stem	WELL DEPTH: N/A	BORING DIAMETER:
14:00	1						● B-9	DRILL F					WELL MATERIAL: N/A	FILTER PACK:	SCREEN SLOT SIZE:
14	Former U	ST L	oca	tion	n		D-7	Ed:	Mitc	hel			N/A	N/A	N/A
								WELL S	EAL:	ce	mer	nt / bento	onite		
FINISH	ž	SAN	MPL	INC				-		TIMAT				split spoon	
	WELL CONSTRUCTION DETAIL			7.7	3			OVM READING (PPM)				GRAPHIC LOG	MONITORING INSTRUME	AL: PID	
	STRU	BLOWS/6" INTERVAL	Æ	RECOVERY	ANALYTICAL	EL EL	Ec	REA	VEL	P	10	PHIC	FIRST ENCOUNTERED WAT	пек рерти: аррт	rox. 9.5' bgs
13:00	WEL	38	DRIVE	REC	AN.	WATER	DEPTH (PEET)	OVY.	GRAVEL	SAND	FINES	28	STATIC WATER DEPTH - I	DATE:	
7		-										0,0,0,0,0	Gravel / Sub	ograde Fill (G	(W)
							1 —						Graver / But	grade I III (C	"")
							2 —								
TART	/				-		3 —						Gray clayey	silt (MH), M	loderate Plasticity
6/11/03 DRILLING/WELL CONSTRUCTION: START							4-						Moist, no oc	or	
6					$\vdash$										
STE							5 —								
SNO.							6 -								
BLL							7 —						Brown silty	sand (ML), N	Moderate Plasticity
3/8							8 —						Moist, no o	dor	
T.			-		Н	_				-					
PR		P P	666	6		¥	9 —								
03		P	6	6	X		10 —								
11		_	-		Н		11 —								
9							12 -								
0															
Ser			-		H		13 —	-							
Locicero					Ħ		14 -								
A. L					H		15 —				-	-			
1					H		16 -								
LOGGED BY:							17 —					1			
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3							18								
					H		19 —								
1			-		H		20 —					-			
							21 —								
			-	-	H			-				-			
							22 —	-							
							23 —								
		-	+	-	H		24 —		-	-		-			
							25 —								
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			F	F	П		26 —				-				
BY:							27 —								
VED			-	-	H		28 —			-	+	-			
APPROVED BY:			1				29 —								
~			+	-	H				-	-		-			
							30 —								an passaulting of the control of the



## Calculation of Residual Sorbed-Phase TPHg and TPHd Contaminant Mass Indianola Market, Eureka, CA

Residual Sorbed-Phase TPHg (Area 1)

Mean TPHg conc. (mg/kg)	A (ft2)	h (ft)	V (ft3)	p (lbs/ft3)	TPHg mass (lb)
723.0	780	10	7,800.00	100	563.94
			Total TPHg (	gals)	92.45

Residual Sorbed-Phase TPHd (Area 1)

Mean TPHd conc. (mg/kg)	A (ft2)	h (ft)	V (ft3)	p (lbs/ft3)	TPHd mass (lb)
215.0	780	10	7,800.00	100	167.70
			Total TPHd (	gals)	27.49

Sorbed-Phase TPHg Removed During Overexcavaion (Area 2)

Mean TPHg conc. (mg/kg)	A (ft2)	h (ft)	V (ft3)	p (lbs/ft3)	TPHg mass (lb)
723.0	211	10	2,110.00	100	152.55
			Total TPHg (g	gals)	25.01

Sorbed-Phase TPHd Removed During Overexcavaion (Area 2)

Mean TPHd conc. (mg/kg)	A (ft2)	h (ft)	V (ft3)	p (lbs/ft3)	TPHd mass (lb)
215.0	211	10	2,110.00	100	45.37
			Total TPHd (g	gals)	7.44

A = Area

h = thickness

V = volume = A \* h

p = soil density (assume 100 lbs/ft3)

TPHg mass = V (ft3) \* p (lbs/ft3) \* Mean TPHg conc.

The square footage area for the calculation of estimated residual sorbed-phase TPHg and TPHd excludes the previously excavated area of the former USTs

#### Calculation of Residual Dissolved-Phase Contaminant Mass January 2003 and October 2005 Indianola Market Project No. NC-18

### Residual TPHg January 2003

Residual TP	Hg (zone 1)	TPHg conc	entrations	s >1,000 µ	ıg/L		
TI	PHg mean	A	h	n	V	TPHg mass	TPHg mass
	(mg/L)	(ft <sup>2</sup> )	(ft)		(ft <sup>3</sup> )	(ft³-mg/L)	
	(mg/L)	( )	(11)		(11)	(It -IIIg/L)	(lb)
	1 400						
	1.400	424	20	0.35	2,968	4,155	0.259
Residual TPI	Hg (zone 1)	TPHg conce	entrations	s <1,000 µ	ig/L and >10	00 μg/L	
	Hg mean	A	h	n	V	TPHg mass	TPHg mass
	(mg/L)	$(ft^2)$	(ft)		(ft³)	(ft³-mg/L)	
	(mg/L)	(11)	(11)		(11)	(It -Ing/L)	(lb)
	0.320	1,004	20	0.35	7,028	2,249	0.140
					Total TPH	g Mass (lb)	0.4
						g Vol. (gal.)	0.07
					Total IIII	g von (gan)	0.07
Darld Arms	DE I	2002					
Residual MT	BE January	2003					
Residual MT	BE (zone 1)	MTBE con	centratio	ns <10,00	00 and >1,00	00 μg/L	
MT	BE mean	A	h	n	V	MTBE mass	MTBE mass
	(mg/L)	$(ft^2)$	(ft)		(ft <sup>3</sup> )	(ft³-mg/L)	
	(IIIg/L)	(24)	(11)		(10)	(It -IIIg/L)	(lb)
	1 000						
	1.900	570	20	0.35	3,990	7,581.0	0.47216
Residual MT	BE (zone 2)	MTBE con	centratio	ns <1,000	μg/L and >	100 ug/L.	
	BE mean	A	h	n	V	MTBE mass	MTBE mass
	(mg/L)	(ft²)	(ft)		(ft <sup>3</sup> )	(ft³-mg/L)	
	(IIIg/L)	(11)	(11)		(11)	(It -IIIg/L)	(lb)
	0.320	2,147	20	0.35	15,029	4,809.3	0.29953
Residual MT	BE (zone 3)	MTRE con	centratio	ns <100 u	o/L and >10	ug/L	
	BE mean	A	h	n	V	MTBE mass	MTDE
				п	0.00		MTBE mass
	(mg/L)	$(ft^2)$	(ft)		$(ft^3)$	(ft³-mg/L)	(lb)
	0.0320	3,805	20	0.35	26,635	852.3	0.05308
Residual MT	RE (zone 4)	MTRE con	centration	ns <10 ma	/L and >1ua	/1	
	BE mean				_		) (TDT
		A (02)	h	n	V (03)	MTBE mass	MTBE mass
(	(mg/L)	$(ft^2)$	(ft)		(ft³)	(ft³-mg/L)	(lb)
	0.0032	3,761	20	0.35	26,327	84.2	0.00525
					Total MTD	E Mass (lb)	0.0
							0.8
					Total MTB	BE Vol. (gal.)	0.14

### Calculation of Residual Dissolved-Phase Contaminant Mass January 2003 and October 2005

Indianola Market Project No. NC-18

#### Residual TPHg October 2005

TPHg mean	A	h	n	V	TPHg mass	TPHg mass
(mg/L)	$(ft^2)$	(ft)		$(ft^3)$	(ft³-mg/L)	(lb)
0.330	737	20	0.35	5,159	1,702	0.106
				Total TPH	g Mass (lb)	0.11
				Total TPH	lg Vol. (gal.)	0.02
esidual MTBE October	r 2005					
Residual MTBE (zone 1)	MTBE cor	centratio	ns <1,000	μg/L and >	100 μg/L.	
MTBE mean	A	h	n	V	MTBE mass	MTBE mass
(mg/L)	(ft²)	(ft)		(ft³)	(ft³-mg/L)	(lb)
0.370	489	20	0.35	3,423	1,266.5	0.07888
esidual MTBE (zone 2)	MTBE cor	centratio	ns <100 µ	ıg/L and >1(	) μg/L	
MTBE mean	A	h	n	V	MTBE mass	MTBE mass
(mg/L)	(ft²)	(ft)		(ft³)	(ft³-mg/L)	(lb)
0.0320	2,307	20	0.35	16,149	516.8	0.03219
esidual MTBE (zone 3)	MTBE cor	centratio	ns <10 μς	g/L and >1μg	g/L	
MTBE mean	A	h	n	V	MTBE mass	MTBE mass
(mg/L)	(ft²)	(ft)		(ft³)	(ft³-mg/L)	(lb)
0.0032	4,814	20	0.35	33,698	107.8	0.00672
				Total MTBE Mass (lb)		0.12
				Total MTI	BE Vol. (gal.)	0.02
A = Area						
= thickness				TPHg = To	tal petroleum hy	drocarbons as
V = volume = A * h				MTRF = N	fethyl tertiary bu	tyl ethyr

V = volume = A \* h

n = soil porosity (assume 35%)

TPHg mass = V (ft3) \* Mean TPH conc. (unitless)

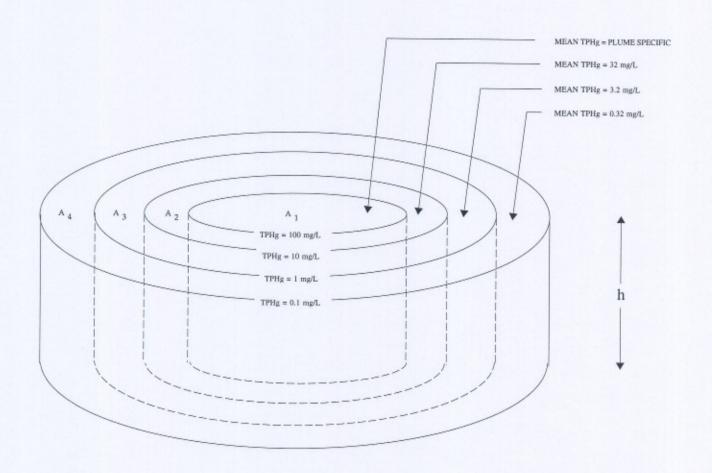
MTBE mass = V (ft3) \* Mean TPH conc. (unitless)

lb = pound

mg/L = milligrams per liter

MTBE = Methyl tertiary butyl ethyr gal. = gallons ft. = foot

# MODEL FOR CALCULATING RESIDUAL DISSOLVED CONTAMINANT MASS (TPHg)



TPHg mass (ft  $^3$ -mg/L) =  $\sum_{1}^{n} V_{X}$  (mean TPHg concentration<sub>X</sub>)

Convert TPHg mass to (lbs) =  $(ft^3-mg/L)$  (28.31 L/ft<sup>3</sup>) (0.000001 kg/mg) (2.2 lbs/kg) where,

$$V_X = A_X(h) n$$

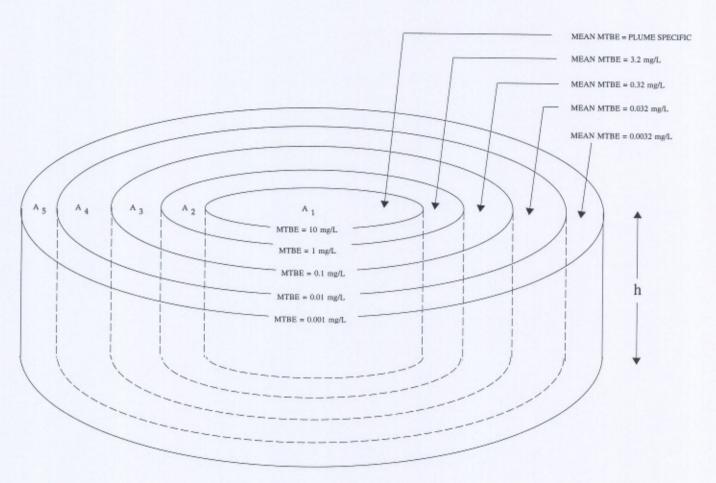
 $A_X$  = Area between isoconcentrations measured by planimeter

h = Thickness of dissolved contaminant plume

n = Porosity of saturated zone soil

Model assumes that contaminant concentrations decrease logarithmically from source. Thus, log based formula was used to calculate mean contaminant concentrations.

# MODEL FOR CALCULATING RESIDUAL DISSOLVED CONTAMINANT MASS (MTBE)



MTBE mass (ft  $^3$ -mg/L) =  $\sum_{1}^{n} \bigvee_{X}$  (mean MTBE concentration  $\bigvee_{X}$  Convert MTBE mass to (lbs) = (ft  $^3$ -mg/L) (28.31 L/ft  $^3$ ) (0.000001 kg/mg) (2.2 lbs/kg) where,

$$V_X = A_X(h) n$$

A x= Area between isoconcentrations measured by planimeter

h = Thickness of dissolved contaminant plume

n = Porosity of saturated zone soil

Model assumes that contaminant concentrations decrease logarithmically from source. Thus, log based formula was used to calculate mean contaminant concentrations.

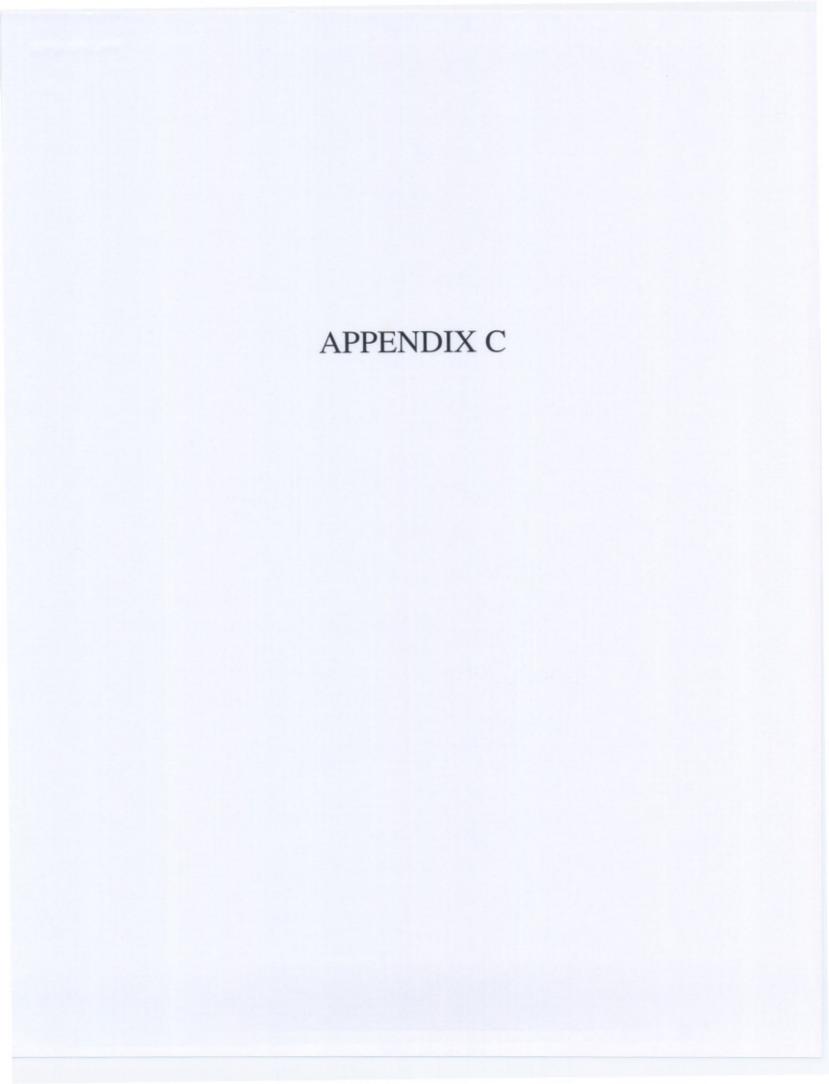


Chart 1 Indianola Market 7769 Myrtle Avenue Eureka, California Project No. NC-18

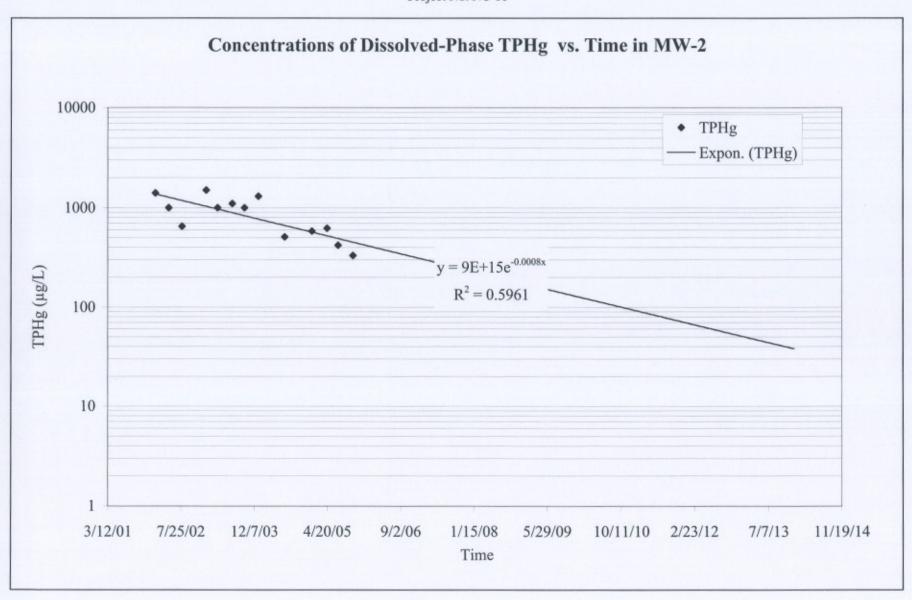


Chart 2 Indianola Market 7769 Myrtle Avenue Eureka, California Project No. NC-18

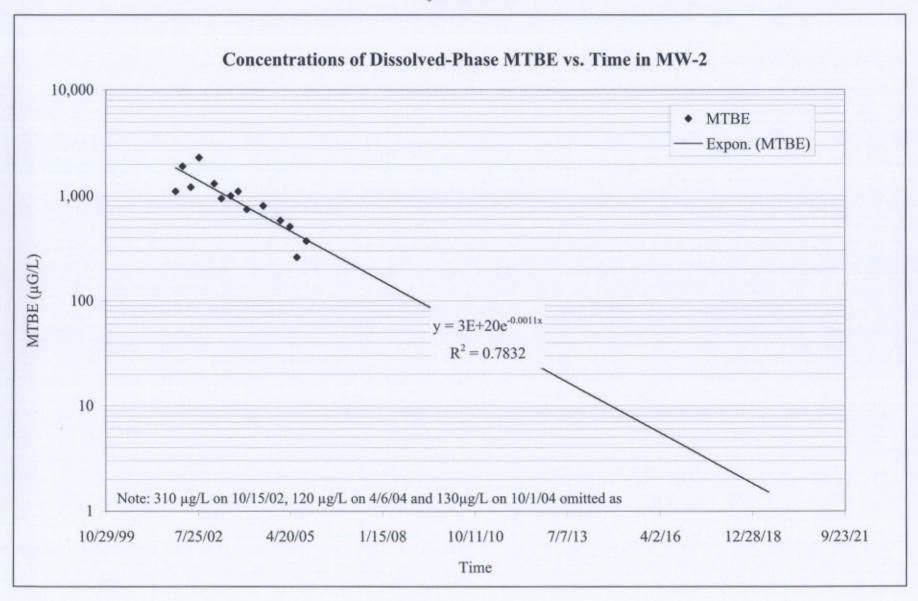


Chart 3 Indianola Market 7769 Myrtle Avenue Eureka, California Project No. NC-18

